

AN OPERATIONAL LANCHESTER-TYPE MODEL OF
SMALL-UNIT AMPHIBIOUS OPERATIONS.

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THESIS

AN OPERATIONAL LANCHESTER-TYPE MODEL OF
SMALL-UNIT AMPHIBIOUS OPERATIONS

by

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September 1981

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An Operational Lanchester-Type Model of
Small-Unit Amphibious Operations

by

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This thesis presents an operational Lanchester-type model of small-unit amphibious operations. This relatively simple model has been developed to demonstrate the basics of model building to the beginning student interested in amphibious warfare. The model is a time sequenced, deterministic, force-on-force combat model that is implemented on a digital computer. A brief discussion of considerations for modeling amphibious operations is given. The details of the model are presented for a specific amphibious-warfare scenario. Additionally, a computer terrain-contour-line plotting program is provided to assist the combat modeler to fit a parameterized-terrain to real terrain.

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I. INTRODUCTION

During the past several decades, combat models have been widely used to support military decisions. As the art of combat modeling becomes more advanced, combat modelers are continuously building more and more complicated models. To the beginning modeler, the ability to understand how those models operate is difficult, if not impossible. It is the purpose of this thesis to develop a simple amphibious-operations model that will demonstrate the basics of model building to the beginning student interested in amphibious warfare. In the broadest sense, an amphibious operation is a combined-arms operation which includes all forms of combat--land, air, sea. This thesis will limit itself to the small-unit amphibious operation.

This project started with two basic models: one was developed as the auxiliary model for the evaluation of design and employment alternatives for the LVA (Landing Vehicle Assault) in the thesis of David Larkin Chadwick (September 1978). The other is the Smoler-Mills model which was developed in the thesis of Josef Smoler (September 1979) and enriched in the thesis of Glen Mills (September 1980).

In Chapter II, general considerations for modeling amphibious operations are briefly discussed. Then, a small-scale computer-based Lanchester-type amphibious-operations model is presented, including analytical details of the algorithms used

to represent each of the combat processes considered. Although the model was developed for a specific scenario, it is sufficiently general in design so that it can be adapted to other small-scale amphibious-operations scenarios with only relatively few modifications.

II. GENERAL CONSIDERATIONS FOR MODELING AMPHIBIOUS OPERATIONS

A. CHARACTERISTICS OF AMPHIBIOUS OPERATIONS

In order to model an amphibious operation, it is first of all necessary to understand what is going on in a real amphibious operation. Only after one knows the details of what is happening in such a complex combat operation, can one begin to sift out the cluttering details and make valid simplifying assumptions to come up with a tractable model.

One of the key characteristics that serves to distinguish amphibious operations from other types of military operations is that a complete military force must be transferred ashore in an orderly manner under the constant pressure of actual or potential attack from hostile forces. Because the over-all amphibious assault requires precise and timely execution, the various component operations must be carried out in a planned sequence (especially early in the assault) according to a strict schedule. This sequence and these schedules, however, must be sufficiently flexible to permit rapid changes in line with unexpected development afloat and ashore.

The notable success of amphibious operations during and after World War II is testimony to the fact that, with proper planning and organization, this dual problem can be solved. In today's environment, it is well known that the modern battlefield will be dominated by highly lethal weapons. This has raised serious questions about the survivability of amphibious

forces. On the other hand, the long-range, high-speed assault potentially gives one the capability to launch assaults from far out to sea, land at times and places of one's choosing, and carry more firepower to accomplish the amphibious assault with greater safety for ships and men. Use of some type of combat model is the only way to explore such issues today. In order to build such a combat model of an amphibious operation, it is necessary to develop and consider detailed and specific information on individual tactical and support elements of the landing force, on the size, numbers, and characteristics of the equipments of these elements, and on the sequence of movement of these elements.

The amphibious operation is a combined operation, the entire spectrum of activities involved in an amphibious operation includes:

- pre-assault bombardment by ships and aircraft
- sea mine clearance
- attack on ships by enemy aircraft and cruise missile
- ship-to-shore movement
- surface assault landing
- helicopter operation
- ground combat between maneuver units
- artillery and naval gunfire support
- tactical aircraft support
- mine warfare (sea and land).

While an amphibious operation is one of the most complex of all military operations, defending against it is even more

complex: it is absolutely impossible for an enemy to defend all coastal areas at all times. The flexibility to conduct helicopter-borne vertical assault and surface-borne assault simultaneously will greatly enhance the complexity of defending against an amphibious assault.

Airborne troops and supplies were valuable during the Second War, and further developments in that direction are under way. But whether or not modern airborne tactics and techniques have supplanted (in a practical sense) seaborne assaults (such as those used from 1942 through 1945 in the Pacific and elsewhere), it should be noted that the military problem of landing forces on shores held by an enemy remains. The emphasis in the future will most likely continue to be on having the ability to project forces from the sea onto a hostile shore and to hold such a beachhead.

B. MODELING APPROACH

All models of military operations must abstract from the real world. Since it is obvious that an engagement between modern military forces is a very complicated process, one has to abstract, aggregate, and interpolate in order to scale a combat process down to manageable size for modeling purposes. A variety of modeling approaches are available. These range from simple Lanchester-type models to highly complicated, computer assisted, high-resolution simulations in which the actions of each individual combatant are traced through a combat scenario second by second. Between these two extremes are

other approaches covering the whole spectrum of land combat, from one-on-one duels to theater-level models covering huge geographical dimensions.

There are basically four different types of combat models: war games, analytical (or mathematical), simulations and some combination of these first three types. According to Bonder [Ref. 2], war games are not a feasible mechanism for analyzing a broad spectrum of system alternatives in a responsive manner to meet a planning cycle requirement. However, they are diagnostic in the sense that they reveal problems that need to be resolved with future systems, and are a viable mechanism for training decision makers. Analytical models seek to describe the combat process mathematically. They simplify the conduct of sensitivity analysis and provide an increased ease in interpreting results, since the dynamics of the combat process are contained in readily examined equations. Analytical models of any degree of complexity usually do not yield convenient analytical solutions but require numerical approximation methods. Simulation is the most widely used technique in military system analysis. Simulation can generally produce very useful data, which are needed for further analysis, and sometimes for planning itself. However, the large amount of detail contained in most Monte Carlo simulations makes it difficult to use as the sole vehicle to single out those systems capabilities, tactics, and environmental conditions which significantly contribute to or delimit the system's effectiveness. Since, as we have seen above, no one type of combat model

is unconditionally preferred to another, it is proposed that a combat model should be selected or designed based on a specific scenario and upon analytical requirements.

In most cases, detailed models are more credible to decision makers. However, for many people such detailed models of large-scale combat operations are far too complicated to be understood, require too much input data, and (in general) are not responsive enough. When one looks at computer storage and run time requirements for even the smallest high resolution model, it is easy to see why a high resolution model of a corps or theater is presently impractical, and is likely to remain so. In order to avoid the complexity of the large-scale model and to better understand land combat there is a growing trend among analysts to combine small unit and large unit models in such a way that the output data of a high-resolution small unit combat model is used as the input data for a low-resolution large unit model. The obvious drawback of this hierarchical-modeling approach is that any errors in the small unit models will be carried through, and possibly multiplied, as the process proceeds from model to model. In the large units the emphasis has been away from simulation and towards detailed Lanchester-based models.

So far the emphasis has been adding more and more detail to the high resolution models so as to pick up as many interactions as possible. No matter how much detail is added to the small-unit simulation, it seems impossible that reality will ever be matched exactly. With this in mind, it is proposed

that a well-constructed Lanchester-based model of small unit engagements could give results that are just as valid as the results of a high-resolution simulation.

III. THE MODEL

A. GENERAL

1. The Scenario

The scenario considers an amphibious-landing team, consisting of reconnaissance, a light infantry unit, and landing-assault vehicles. This team is part of an Amphibious Task Force (ATF), and it disembarks from ships that are on station over the horizon from the selected landing site. The assault vehicles, after transmitting from the amphibious shipping to the designated area for the landing formation, form into conventional landing waves at a distance offshore which is greater than the effective range of the direct-fire weapon systems of the shore-defense force. During the ship-to-shore movement the defender's anti-tank guided missile and improved gunnery system respond to the landing. Naval gun-fire ships provide fire support for the assault team during the ship-to-shore movement and the initial stages of landing.

As the assault vehicles reach the beach, they (together with the assault vehicles and any weapons landed by landing vehicles) launch an attack on the enemy shore defense positions. The defenders occupying those positions fight until their losses exceed a maximum permissible amount. The attacking force, however, continues the assault irregardless of losses incurred. Once the shore assault has been completed, the landing force with tactical mobility moves inland to

carry out the tasks, while the enemy prepares to mount a counter attack.

The attacker may engage the advance force of the defender's initial counter attack force on the way to move inland. The advantage will likely go to that force which has gained the initiative (i.e., the landing force) provided it can maintain its momentum.

2. General Description of the Model

The model developed in this thesis is a time sequenced, deterministic, force-on-force computerized model, coded in FORTRAN. The model conducts the battle in uniform time steps of 10 seconds each. Figure 1 shows the general scheme for the sequence of events in the model. The model simulates two main phases in the amphibious operations: (I) the amphibious-assault phase, and (II) the subsequent ground attack. The framework and the logical interrelationships of these two phases will be discussed in the following subsections.

B. THE AMPHIBIOUS ASSAULT PHASE

1. General

In this phase the model considers attrition between the shore-defense force and the landing-assault force during its water-borne movement and subsequent assault to shore. The model aggregates the various actual combat organizations involved in the waterborne phase of the amphibious operation into several homogeneous combat units. Each of these units is characterized by certain relative offensive and defensive

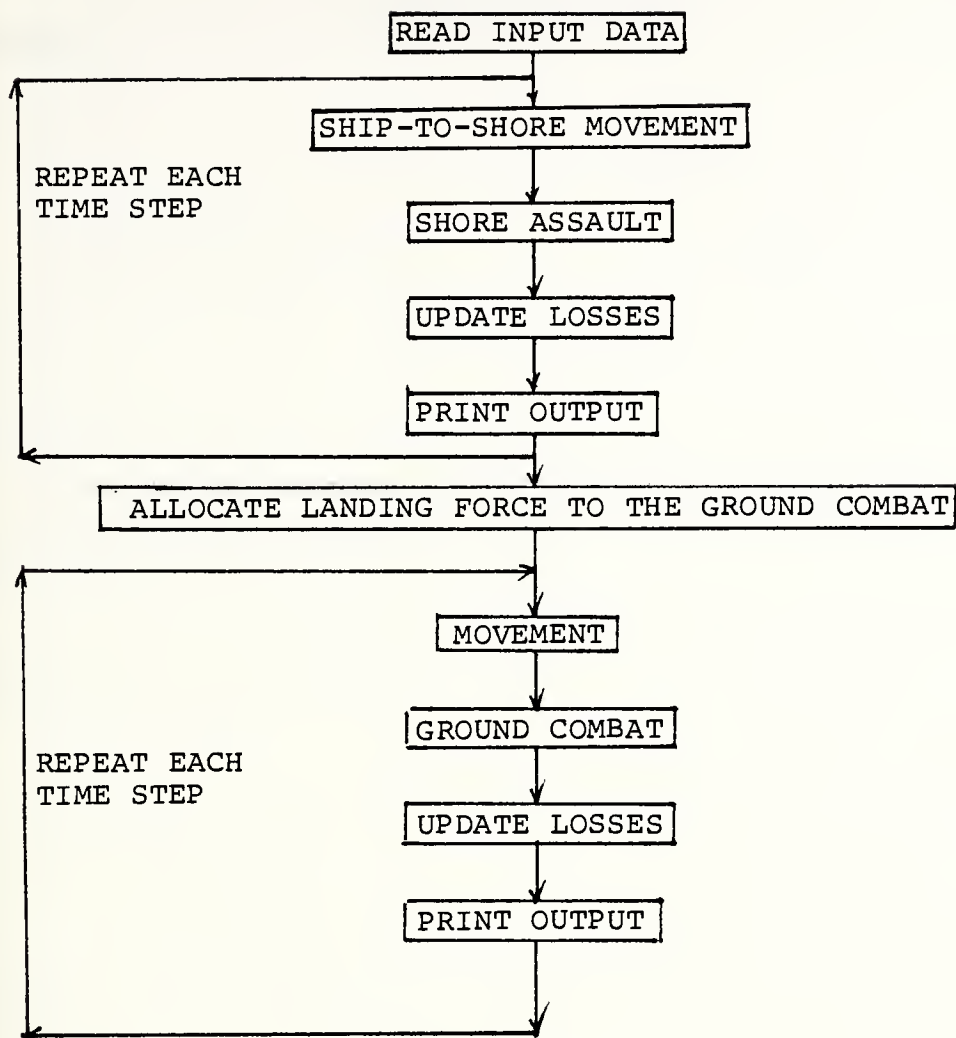


Figure 1. General Scheme for the Amphibious Operation Model

capabilities. The following table illustrates the combat organizations that were explicitly modeled. The combat strength of each unit was represented by the state variables indicated.

| <u>combat organization</u> | <u>state variable</u> |
|--|-----------------------|
| Shore Defense--TANK assets | DT |
| Shore Defense--ATGM assets | DS |
| Incoming assault waves of LVA representing waves 1 through 5 | WV(I), I = 1,2,3,4,5 |
| A cumulative combat force comprised of those Marine ground units which have arrived at the beach and have debarked the LVA | TLF |
| Fire Support Assets of The Amphibious Task Force | ATFFS |

The initial strength in each of the above units is input data to the model.

The schematic of the method of employment for the LVA in the ship-to-shore phase of an amphibious assault is shown in Figure 2. It is assumed that the conventional landing formation composed of waves of landing vehicles will be used as prescribed by current doctrine. The movement of assault vehicles to the beach is simulated using a time step approach. At each time increment the positions of vehicles are updated.

The tactical interrelationships which exist between various combat units are illustrated in Figure 3. Assuming that in such a future amphibious operation the attrition of

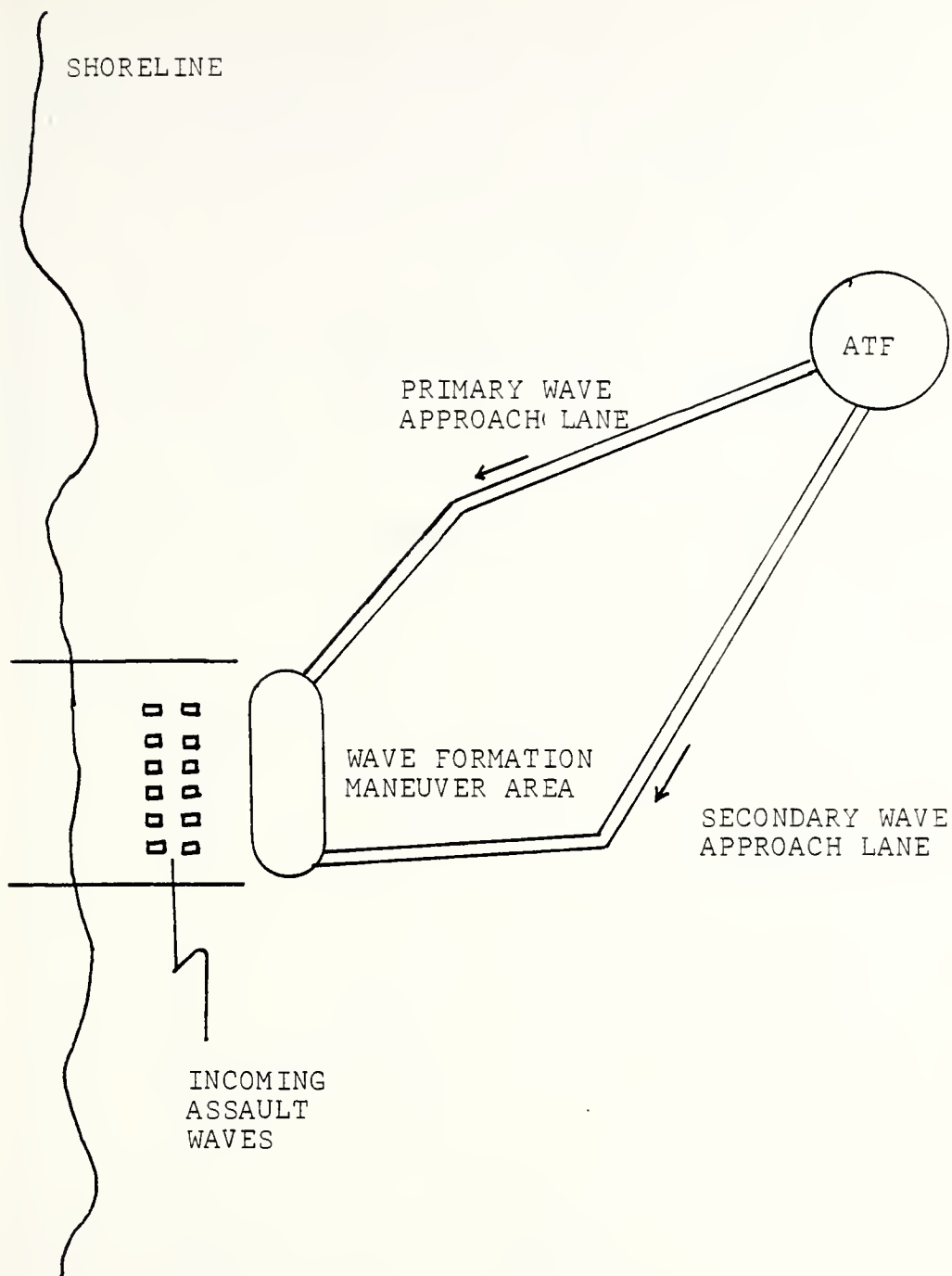


Figure 2. Concept of Ship to Shore Movement

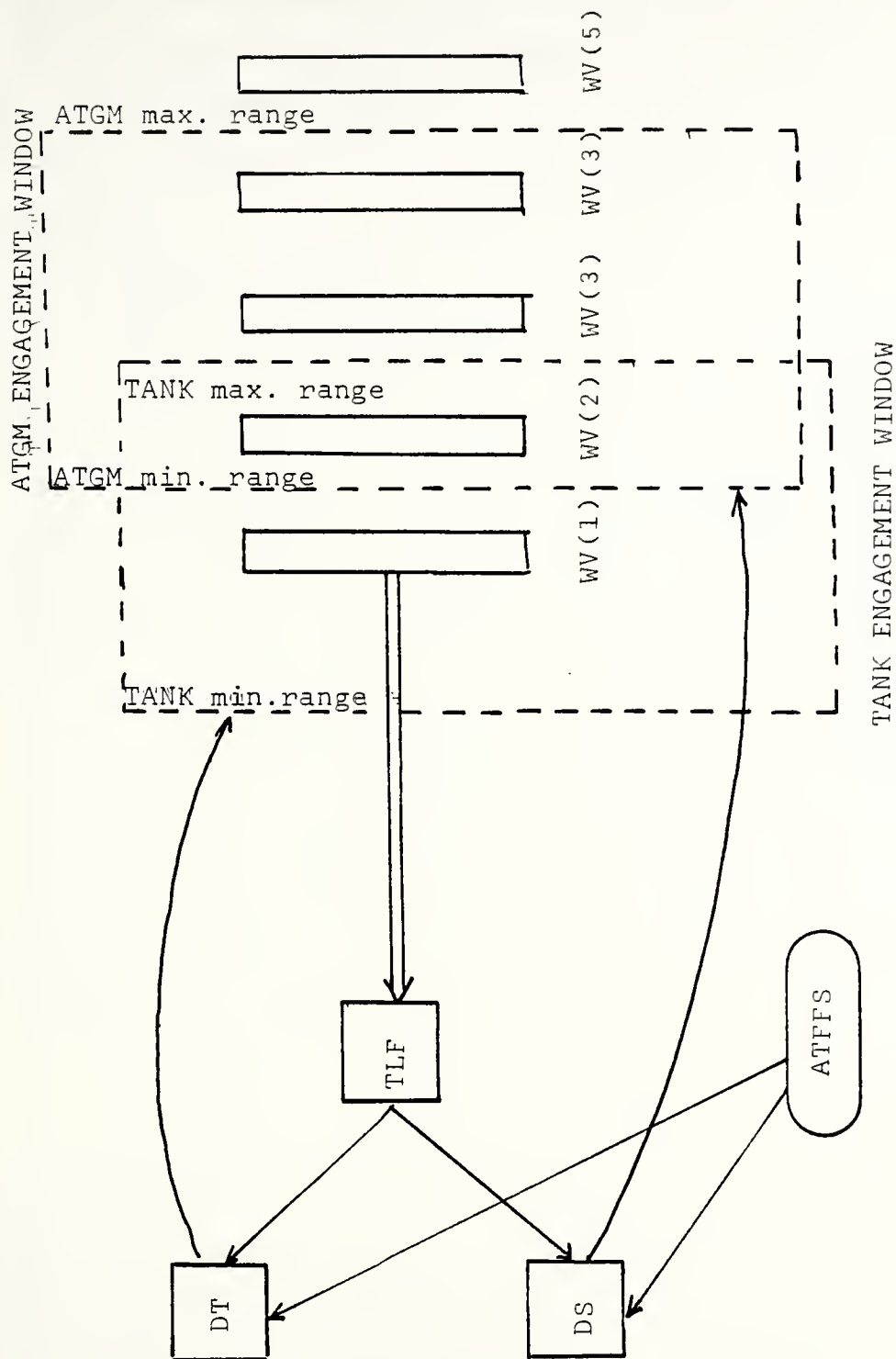


Figure 3. Schematic of Tactical Interrelationship between Combat Units during Amphibious Assault Phase

incoming landing vehicles would be dominated by the effects of shore defense direct-fire weapon systems (specifically, tank and anti-tank guided missile (ATGM) assets), the model essentially omits the effect of the defensive indirect fire capabilities.

2. Attrition Process

The model represents the attrition of all combatant units as a deterministic process. The primary consideration in the ship-to-shore movement of incoming waves of assault vehicle is the attrition effects upon those waves due to the direct fire weapon assets ashore. The attrition of each wave utilizes Lanchester "aimed-fire" equations with variable attrition-rate coefficients.

The classical Lanchester hypothesis for aimed-fire attrition (combat under "modern condition") is that the casualty rate of a unit is proportional to the "size" of the opposing forces. If the unit "A" is being engaged by "D", this may be expressed by the differential equation:

$$\frac{dA}{dt} = - \text{BETA}_{DA} \times D$$

The proportionality constant BETA_{DA} is called the Lanchester attrition-rate coefficient. It is assumed that this functional relationship holds for each (firing unit, target unit) pairing over a small time interval dt . The problem then is to determine numerical values for the Lanchester attrition-rate coefficients. In this model, these coefficients were expressed



as the product of the rate of fire (ROF) and the kill probability per round (P_k). Thus,

$$BETA_{DA} = ROF_{DA} \times P(k)_{DA}$$

The rate of fire (ROF) can be expressed as the reciprocal of TBF (Time Between Firings) which can be evaluated by

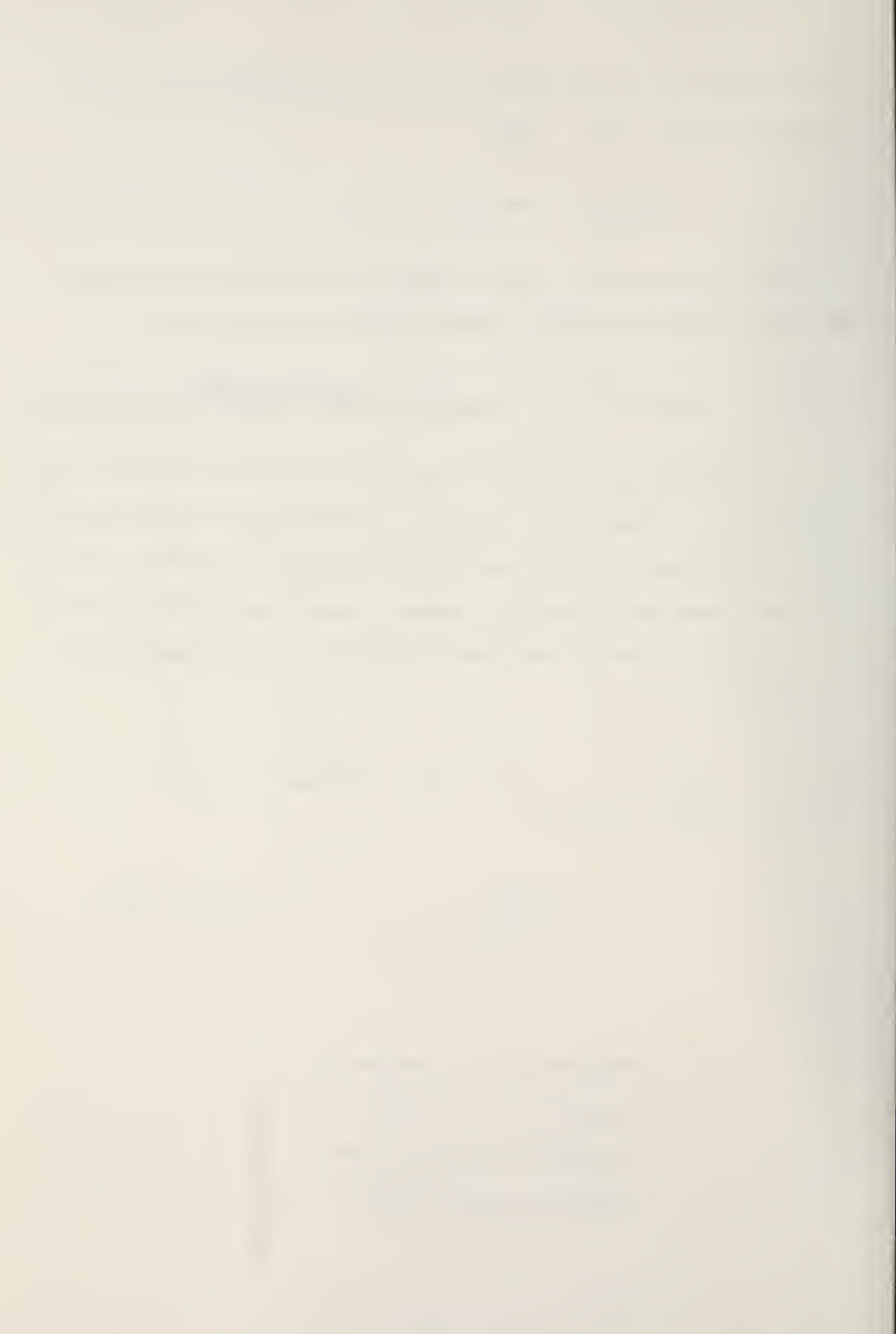
$$TBF = AIM-RELOAD TIME + \frac{TARGET RANGE}{TARGET SPEED + PROJECTIVE VELOCITY}$$

In determining the probability of a vehicle "KILL" per round, it is assumed that a hit by a large caliber projectile would constitute a "KILL" and the two defensive weapon systems addressed would exhibit normal, uncorrelated horizontal and vertical errors. Then the single shot kill probability is given by

$$P(k) = \left[\left(\frac{1}{\sqrt{2\pi}} \right) \int_{(-a-u)/\sigma_x}^{a-u/\sigma_x} \exp\left(-\frac{x^2}{2}\right) dx \right] \cdot \left[\left(\frac{1}{\sqrt{2\pi}} \right) \int_{(-b-v)/\sigma_y}^{(b-v)/\sigma_y} \exp\left(-\frac{y^2}{2}\right) dy \right]$$

where:

- a = semilength of a target
- b = semiwidth of a target
- u = horizontal aiming error
- v = vertical aiming error



σ_x = round-to-round standard deviation in vertical

σ_y = round-tround standard deviation in horizontal

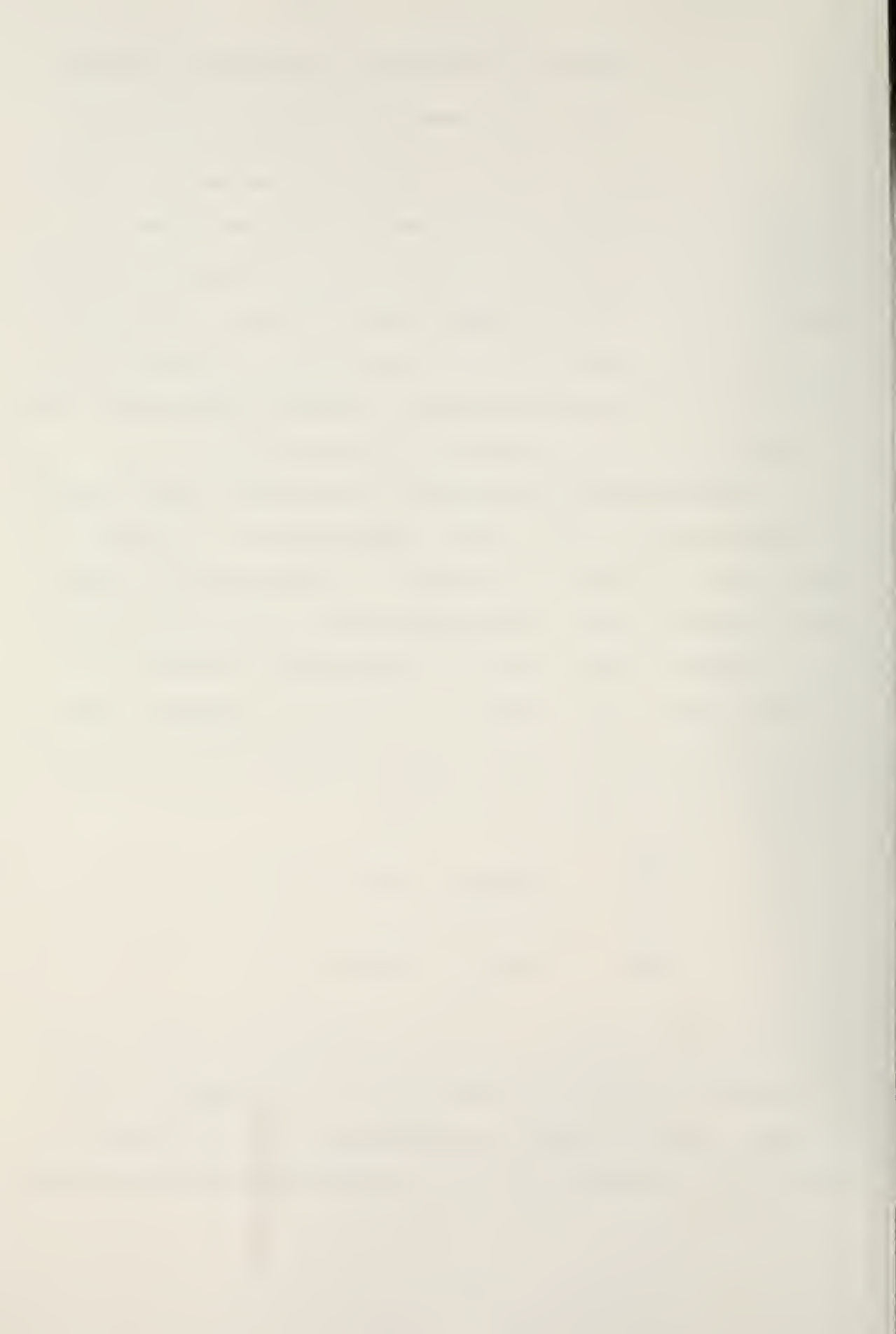
Model functions RNG, HT and SPD are called upon within the model logic to generate the range, height and speed respectively for each assault wave as time is incremented throughout the course of the amphibious assault phase. This information and typical dispersion data (both mean and standard deviation for the tank and ATGM weapons) are then incorporated into the rate of fire and hit probability calculations.

The Amphibious Task Force's fire support assets contribute significantly to the combat effectiveness of the shore defense units. Since it is assumed that the exact positions of the defensive units DT and DS emplaced on shore are unknown to the Amphibious Task Force and consequently the ATF fires into the general areas thought to contain the defensive units. The following Lanchester-type area-fire equations are applied to compute the attrition of DT and DS.

$$\frac{dDT}{dt} = -(\text{ALPHA}_{DT} \times \text{ATFFS}) \times DT$$

$$\frac{dDS}{dt} = -(\text{ALPHA}_{DS} \times \text{ATFFS}) \times DS$$

The combat effectiveness of the ATF fire support assets is to be considered relatively constant during this segment of combat time. Thus the terms in parentheses on the right hand side of these equations are to be considered an input parameter.



Once a particular defensive unit has initiated its engagement of incoming waves it is considered that their fire "gives away" their exact locations. At this point it is assumed that the ATF fires will engage that defensive unit through the use of aimed-fire and the loss rate will be in accordance with the Lanchester hypothesis for aimed fire. That is,

$$\frac{dDT}{dt} = -\text{BETA}_{DT} \times \text{ATFFS}$$

$$\frac{dDT}{dt} = -\text{BETA}_{DS} \times \text{ATFFS}$$

Again, the parameters on the right-hand sides of both these equations are provided as input.

The casualty rates applied against the DT and DS by the Total Landed Force (TLF) are determined by means of the Lanchester aimed-fire attrition rate coefficients by the equations

$$\frac{dDT}{dt} = -\text{WBETA}_{\text{TLF-DT}} \times \text{TLF}_{DT}$$

$$\frac{dDS}{dt} = -\text{WBETA}_{\text{TLF-DS}} \times \text{TLF}_{DS}$$

The computation of these WBETA coefficients is not performed within the model utilizing the detailed rate of fire and $P(k)$ arguments described previously but is required as input. Although the defensive losses are considered significant,

a high level of complexity for computing these coefficients has not been incorporated into the model at this time.

Figure 4 describes the schematic of the attrition process of the amphibious assault phase in the model. The attrition during each time step was computed using the Euler integration method to approximate Lanchester's force-on-force attrition differential equations.

3. Fire Allocation

Each weapon category was assigned an engagement window as illustrated in Figure 3. Only those LVA located within these range windows could be fired upon by the shore defenders. A defensive weapon only engages the two closest incoming waves if more than two waves of LVA are at any time located within the weapon's engagement window. If only one wave of LVA is present in a weapon's engagement window, defensive fires of that particular weapon type will be distributed uniformly against the surviving LVA in that wave.

If two waves of LVA are both contained within the engagement window, defensive fires of that particular weapon type will be distributed according to a tactical allocation submodel. A weighting factor (DEFWT) is utilized in establishing the proportion of the total weapon strength to be allocated against the surviving LVAs in each of the two waves. As an example, if $DEFWT(1) = 2$ and $DEFWT(2) = 1$, then each surviving LVA in the closer of the two incoming waves would be allocated twice as much fire as surviving LVA in the seaward

DIRECT FIRE DT/DS AGAINST FOR EACH INCOMING WAVE I

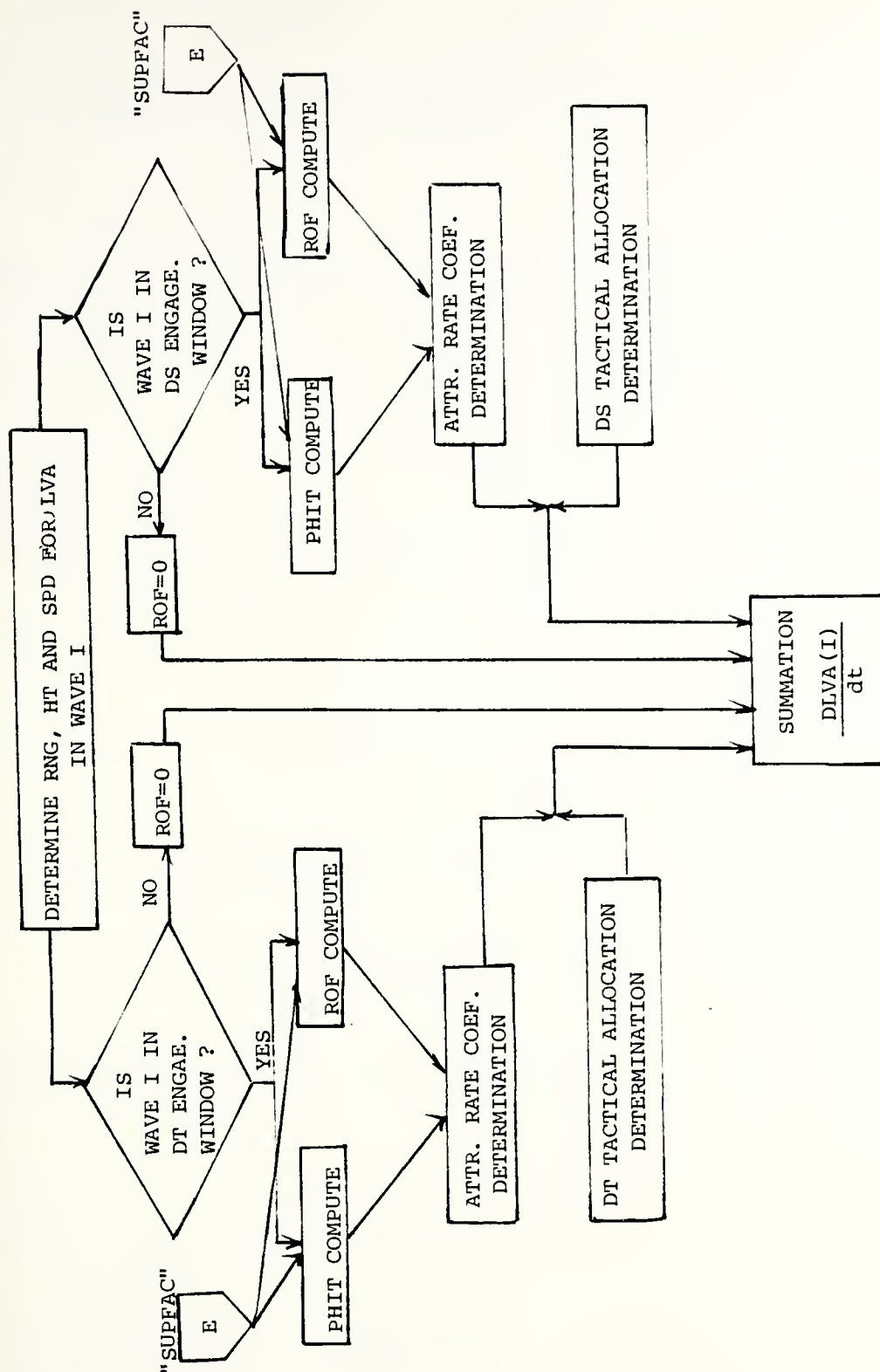


Figure 4. Schematic of The Attrition Process for The Assault Phase

ATTRITION FOR THE SHORE DEFENSE FORCE

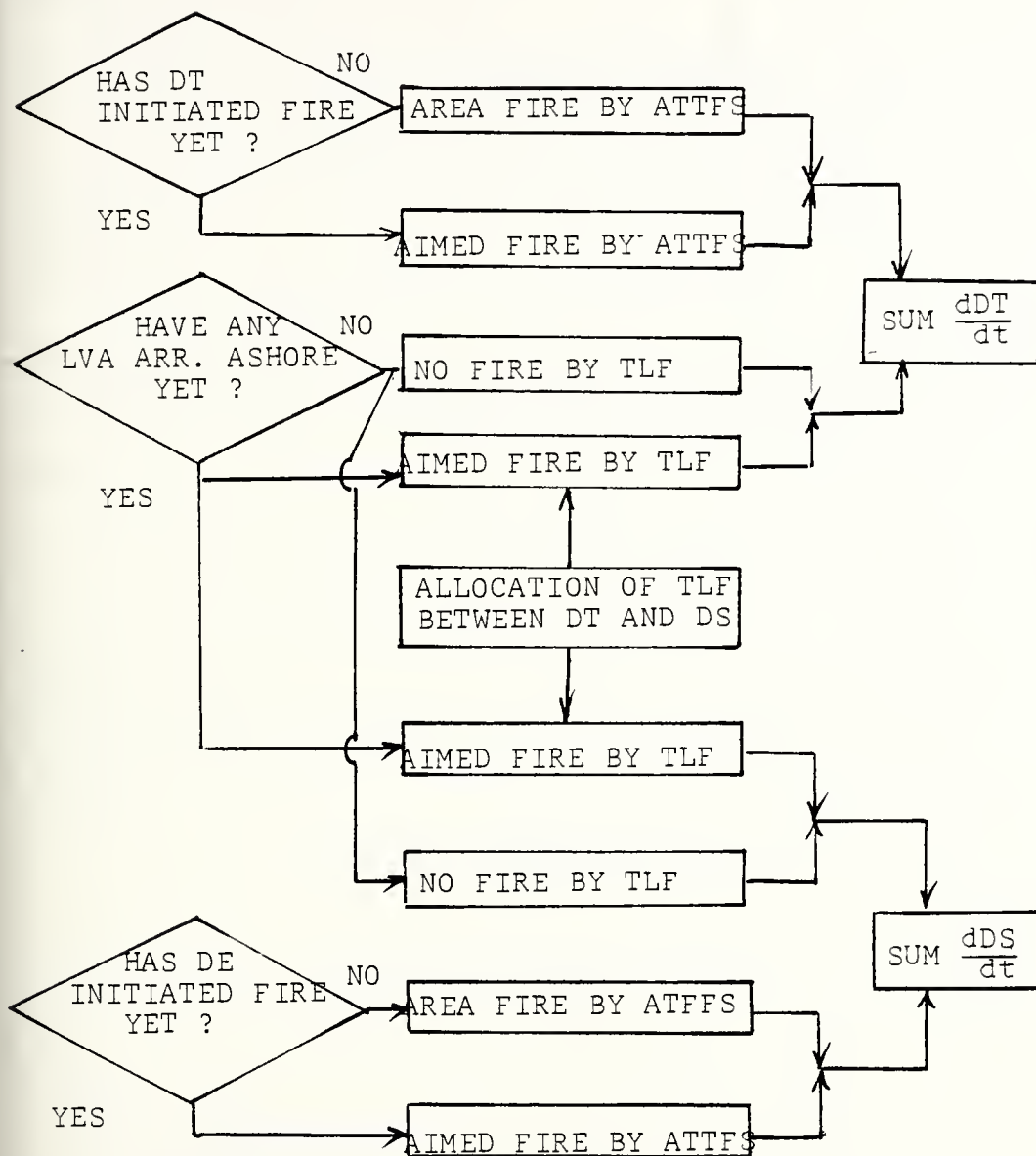


Figure 4.(cont)

wave. For the purpose of these examples, if waves 3 and 4 were both located within the tank engagement window, then the proportion of DT's fire allocated to surviving LVA in wave 3 would be

$$\frac{\text{DEFWT}(1) \times \text{WV}(3)}{\text{DEFWT}(1) \times \text{WV}(3) + \text{DEFWT}(2) \times \text{WV}(4)} \times \text{DT}$$

where WV(3) is the state variable for the current number of survivors in wave 3.

As each assault wave arrives at the beach, the total surviving strength of that wave is transferred to the variable TLF (Total Landed Force). TLF represents a ground combat force equal to that transported by the number of LVA survivors having arrived ashore. Once established, TLF engages the two shore defensive units allocating its fires between the two defensive weapon categories in the same proportion as the number of surviving tanks and ATGM's, that is

$$\text{TLF}_{\text{DS}} = \frac{\text{DS}}{\text{DT} + \text{DS}} \times \text{TLF}$$

$$\text{TLF}_{\text{DT}} = \frac{\text{DT}}{\text{DT} + \text{DS}} \times \text{TLF}$$

4. Suppression

The suppression effects of incoming fire upon each of the defensive units was considered a significant factor with respect to its effect on the survivability of the incoming assault waves of LVA. Generally, the effect of suppression

fire will hinder an individual from observing and firing at the enemy.

It was assumed that suppression would degrade unit effectiveness by increasing the aim-reload time (ARTM) and round-to-round error standard deviation for each weapon system. Hypothesizing that attrition rate is the dominating variable, and therefore, a good indicator of the suppression level, ARTM and such round-to-round errors were assumed to be functions of the force's attrition rate. This is an area, however, requiring further study. Analytically,

$$ARTM_{sup} = ARTM_{nonsup}(1 + GAMMA \times DA)$$

$$ERROR_{sup} = ERROR_{nonsup}(1 + DELTA \times DA)$$

where:

DA = attrition rate for defensive unit due to the effect of AFTTS and TLF

GAMMA = parameter representing relationship between DA and ARTM

DELTA = parameter representing relationship between DA and error standard deviation

This increase of ARTM and round-to-round error (expressed as a standard deviation) decreases the kill probability (P_k) for both defensive weapon categories. Parameter estimation would appear to be the largest problem. But, since determining these parameters in the model is beyond the scope of this thesis, these parameters GAMMA, DELTA are provided as input.

5. The Termination of the Assault Phase

It is assumed that if during the course of the amphibious operation the shore defense forces suffer a cumulative loss in excess of 70% of their initial force strength, the remaining shore defense will try to withdraw, resulting in termination of the engagement.

C. THE INITIATION OF GROUND ATTACK

In the amphibious operation, the landing-force must seize critically-important inland objectives as rapidly as possible before the defenders start to react to the landing. The decision for the initiation of ground attack should be based upon the enemy threat and desired landing-force build-up ashore, among other factors. To model this decision rule, it is assumed that once the landing has begun, the landing-force commander will base his decision about initiation of ground attack primarily on the strength of the landing-force ashore and the shore defender's strength. The criteria for the decision should meet these two conditions:

- (1) The survived landing-force strength has to be greater than the minimum force required to carry out the ground attack.
- (2) The defender's strength must fall below the minimum required to continue coordinated shore defense before breakoff and retreating.

These conditions are then checked after each time step. If all waves landed without reaching the above second conditions, it

is assumed that the next wave group will engage any leftover defenders. Thus, the decision to implement the ground attack is based on the size of the total landed force.

D. THE GROUND ATTACK PHASE

The attacking force which is composed of three subunits of three LVAs armed with TOW antitank missile system attacks along predetermined routes. The defending force is comprised of three subunits of three tanks in a static defense.

The battle takes place on parameterized terrain which will be discussed later. The ground-attack process contains five main subprocesses: (1) movement, (2) detection, (3) fire-allocation, (4) attrition and (5) battle termination. The general flow of the ground attack phase is shown in Figure 5.

1. Movement Process

Every attack unit is advanced to the next interval along a predetermined route unless this unit is destroyed already or is in firing status. To use his own determined routes, the user is required to input the original location of each attacking subunit and from one to ten nodes he wishes each attacking subunit to move through. This information, along with vehicle speed, is used to calculate route intervals that move the attacking unit through each of the designated nodes. The straight line ground distance between the first two adjacent nodes, DIST, is calculated as

$$\text{DIST} = \sqrt{X^2 + Y^2}$$

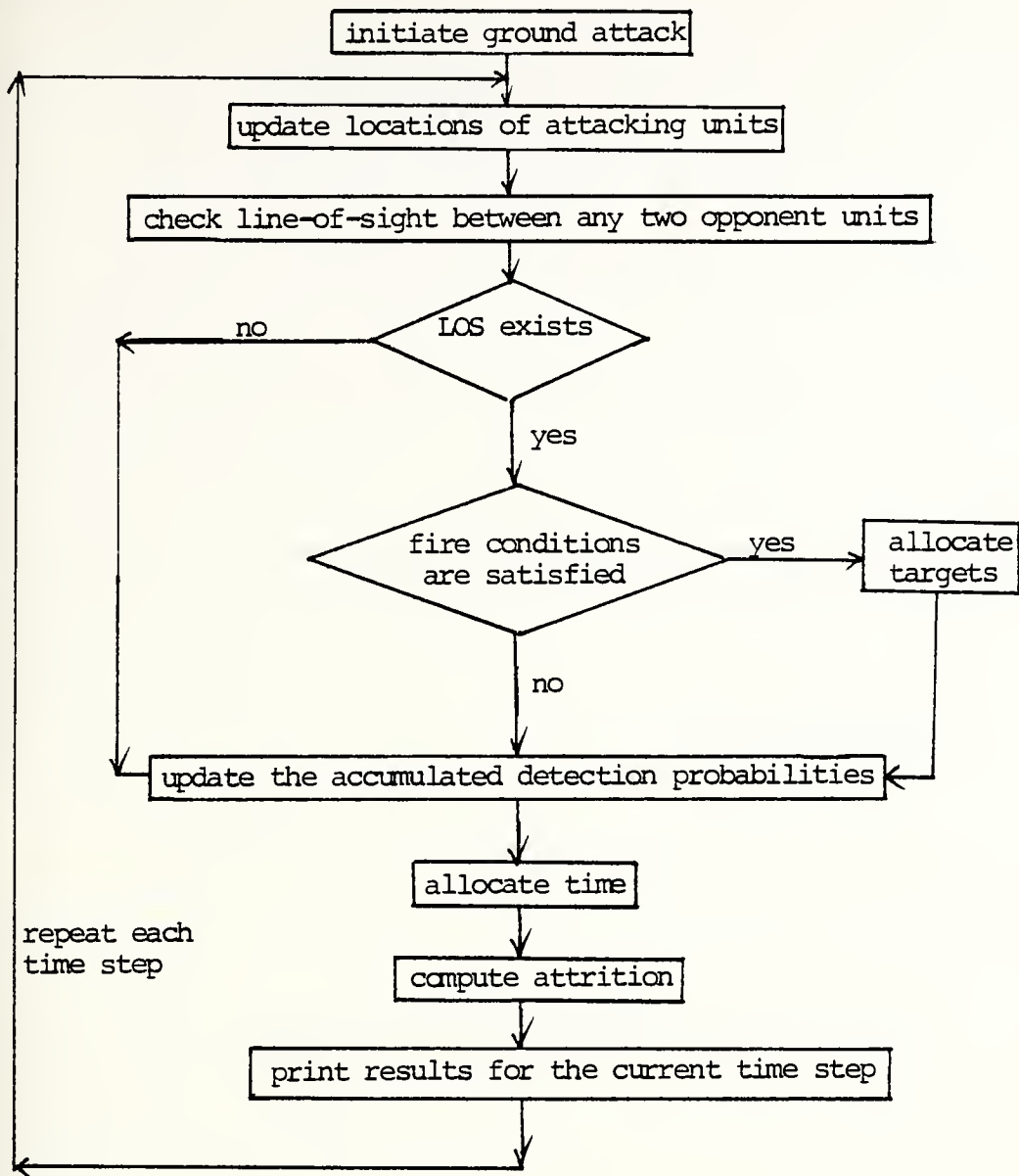


Figure 5. Flow Chart for the Ground Attack Phase

where:

X = distance between two nodes in straight west-east direction

Y = distance between two nodes in straight south to north direction

The angle between the desired direction of movement and straight west to east movement, α , is then calculated. Utilizing these quantities, the distance desired to move during each time step (DST) and the distance to be moved in the X and Y direction (XLN,YLN) is computed. These distances (XLN,YLN) are then added to the coordinates of the previous interval endpoint to determine the coordinates of the next interval endpoint. This process is repeated between the next two nodes until the unit has traversed the entire route.

2. Detection and Fire Allocation

The detection phenomena are modeled in two ways:

(I) non-firing detection, and (II) firing-detection. A non-firing detection can occur as a result of an observer's random search within his designated sector of responsibility. The probability (P_k) that an observer A looking at the direction which enables him to detect a target is computed by integrating the Limicon Function over limits are $\pm 15^\circ$ from the primary direction the observer is looking. The Limicon Function, $f(\theta)$, is the following probability density function:

$$f(\theta) = A + B \times \cos(\theta) \quad -0 \leq \theta \leq 0$$

where:

$$D = \text{assigned sector width}/2$$

$$A = -B \times \cos(D)$$

$$B = \frac{1}{2}(\sin(D) - D \times \cos(D))$$

θ = primary direction observer is looking

Assuming 30° field of view for any observer A target B might be seen only if the observer A is looking at the direction such that $ANGRT \leq \theta \leq ANGLFT$ where:

ANGLE = the absolute value of the angle between the primary direction (IPRDIR) and the observer-target direction (OTANG)

$$\text{ANGLFT} = \begin{array}{ll} \text{angle} + 15^\circ & \text{if } \text{angle} + 15 \leq D \\ D & \text{if } \text{angle} + 15 > D \end{array}$$

ANGRT = angle - 15°

Thus

$$P_k = \text{pr}(\text{ANGRT} \leq \alpha \leq \text{ANGLFT})$$

$$= \int_{\text{ANGRT}}^{\text{ANGLFT}} f(\alpha) d\alpha$$

Given that observer A is looking at the direction, the conditional detection rate (λ_{AB}) is determined by the regression curve [Ref. 11]. The probability that unit j is detected by unit i at time $t + \Delta t$ [$P_{ij}(t + \Delta t)$] is computed according to:

$$P_{ij}(t + \Delta t) = 1 - e^{-\int_t^{t+\Delta t} \lambda(t) dt}$$

$P_{ij}(t)$ can be interpreted as the average fraction of unit i that detects unit j .

The second method of detection played in the model is a so-called firing detection. This phenomena occurs when the following happens: if a firing location is within $\pm 15^\circ$ of an observer's primary direction of observation when he is firing, he is assumed to be detected and is added to the observer's target list. In summary, the following conditions are necessary for unit j to be a target of unit i :

- (a) Line-of-sight must exist between unit i and unit j .
- (b) The range between the two units should be between maximum range and minimum range of the firer's weapon system.
- (c) $P_{ij}(t - \Delta t) > 0$.

The fire-allocation routine determines what fraction of each unit is allocated to fire each target in target list since it is assumed that each fire unit is not restricted to fire at one target. This fraction is determined as a function of the predetermined fire policy and $P_{ij}(t)$. The fire policy is as follows:

| # of target | % of unit i allocated to each target | | |
|-------------|--|--------------------------|--------------------------|
| | 1 st priority | 2 nd priority | 3 rd priority |
| 1 | 100% | | |
| 2 | 80% | 20% | |
| 3 | 80% | 15% | 5% |

The priority of a target is taken to be a function of range only. The fire allocation rule which is used in the model is documented in detail in Smoller's thesis [Ref. 9].

3. Attrition

The attrition process in the ground attack phase utilizes Lanchester "aimed-fire" equation used with variable attrition coefficients. The calculation of the attrition coefficients is accomplished through the use of one of two optional methods. The first option uses the following Bonder-Farrell formula to compute the reciprocal of the expected time to kill. The coefficients, A_{ij} , the rate at which one firer of unit i kills unit j targets are computed according to:

$$A_{ij} = 1/E(T_{ij})$$

where $E(T_{ij})$ is the expected time for one firer of unit i to kill one target of unit j . The $E(T_{ij})$ is computed using:

$$\begin{aligned} E(T_{ij}) = & t_a + t_1 - t_h + (t_h + t_f)/P(K/H) \\ & + (t_m + t_f)/P(h/m) \times ((1-P(h/h))/P(K/H) \\ & + P(h/h) - p) \end{aligned}$$

where:

t_a = time to acquire a target

t_1 = time to fire first round following acquisition

t_h = time to fire following a hit
 t_m = time to fire following a miss
 t_f = time of flight of a round
 P = probability of a first round hit
 $P(h/h)$ = probability of a hit following a hit
 $P(h/m)$ = probability of a hit following a miss
 $P(k/h)$ = probability of a kill given a hit

This formula holds for the conditions that the hit probability of any round depends only on the result of the previous round and no accumulated damage is considered. It is assumed that $P(K/H) = 1.0$ and $P(h/m) = p(h/h) = P$, thus reducing the equation to:

$$E(T_{ij}) = t_a + t_l + t_f + (t_m + t_f)(1-P)/P$$

The second method, called the stochastic method, interprets the attrition rate coefficient, A_{ij}^0 , as a measure of the fighting ability of a unit which has a random phenomena affected by many different factors. It is assumed that the random fighting ability should be distributed between .3 and .8 with the majority of the unit being rated between .5 and .6. A "fitted" distribution to these assumed fighting levels which is devised by Mills is:

$$A_{ij}^0 = -2U^2 + 2U + .3 ; \quad U \text{ is a random Uniform } (0,1) \text{ number}$$

The A_{ij}^0 's are a realization of the random variable denoting a unit's initial fighting capability prior to the battle. Then,

during each time step, a new attrition rate coefficient for each unit is computed using the equation:

$$A_{ij} = \begin{cases} A_{ij}^0 (1 - r/r_e) & ; \text{ for } 0 \leq r \leq r_e \\ 0 & \text{ for } r_e \leq r \end{cases}$$

where:

r_e = maximum effective range of a firer's weapon
 r = current range between firer and target

Utilizing one of the above formulas to calculate A_{ij} 's, the attrition during each time step was computed using the Euler-Cauchy differencing equations to approximate Lanchester's force-on-force attrition differential equations.

4. Termination of Ground Attack

The ground attack is terminated when either:

- (1) One of the two opponent forces is annihilated;
- (2) A distance between each attacking subunit and each defensive subunit which is still engaging becomes "too close";
- (3) Any attacking subunit passes by the flanks of the forward most defensive subunit still in the battle.

The criteria for being "too close" is user input. This allows for flexibility of breakpoint distance for various weapon systems on the battlefield.

E. THE PARAMETRIC TERRAIN

The terrain affects a great deal on detection, mobility, tactics, and intervisibility between weapon systems in ground combat environments. In the model, the battle is simulated on 3 x 4 Km piece of terrain represented as a part of the coastal area east of the Korean Peninsula. It is important to have a terrain representation to emulate actual terrain areas. The model uses the parametric terrain representation method which was proposed by Chris Needle [Ref. 8]. The idea of the parameterized terrain is that the elevation of any hill mass can be represented by a bivariate normal density function. Mathematically, if $f_I(X,Y)$ is a function giving the elevation of the I's hill masses at any X,Y map coordinates on the battlefield, the overall terrain elevation at X,Y is obtained as the positive maximum over all the hill masses,

$$Z = f(X,Y) = \text{maximum } f_I(X,Y) \\ I = 1, \dots, \text{NHILLs}$$

where NHILLs is the total number of hill masses on the battlefield. Then, elevation data is used to compute the existence of line of sight between opposing forces which is a key element in detection process. The model uses the line-of-sight routine which was written by Prof. James K. Hartmann [Ref. 5].

In order to represent a piece of real terrain with parametric terrain, it is necessary to fit hill mass functions $f_I(X,Y)$ to a contour map of the terrain to be modeled. The fitting

process can be done by comparing a computer generated contour map by varying the bivariate normal parameters to the original terrain map. The computer generated terrain map of the battle area is inclosed as Figure 6. Appendix D presents the program listing for plotting a contour map from hill mass functions. This program can be used for the user to fit a specific real terrain which he has in mind into the parameterized terrain.

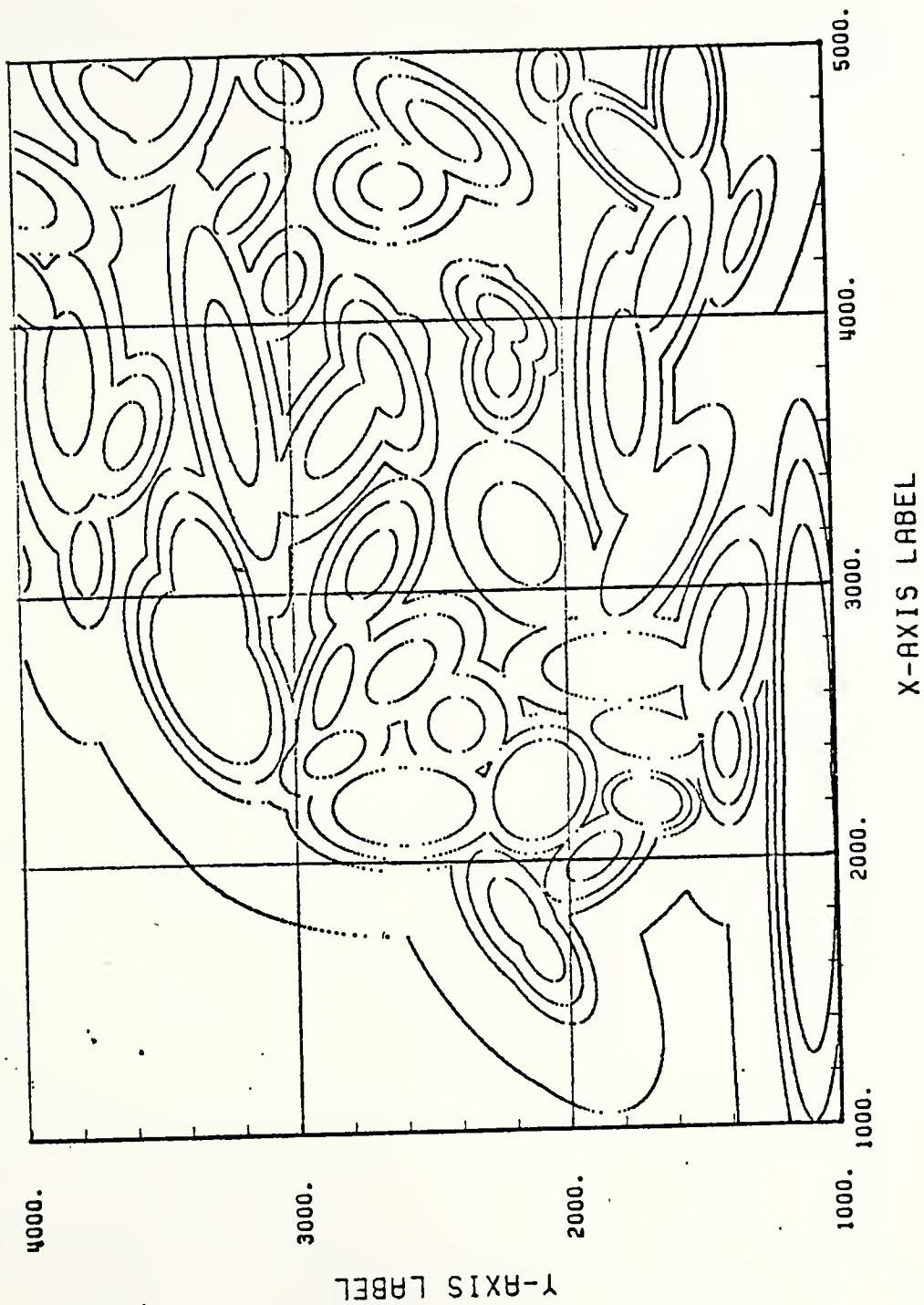


Figure 6. Model Terrain Map

IV. FINAL REMARKS

In order to illustrate basic modeling points for understanding and developing complex-operational amphibious-warfare models, a simplified model (specially tailored to a small-unit-amphibious-operation scenario) has been developed. Although several user options and varieties of modeling techniques have been incorporated into the model, the model should not be viewed as the final product.

There are several areas of model enhancement and enrichment that should be considered in the future. Only the aggregated amphibious task force fire support is played explicitly in the amphibious assault phase. The effect of artillery, naval gunfire and close air support during the various phases of amphibious operations should be added to the model. Ammunition consumption and resupply are considered vital to the success of any military operation, and such aspects should be also added to the model. Enemy forces should be played in greater detail. The movement of reacting enemy force and their dynamic-defensive-position selection are being considered for future model inclusion. A module which considers enemy reaction time, the terrain, and the tactical situation, and which dynamically determines which side is going to take the defensive role, as well as its defensive position, has been proposed to enhance the existing model. Inclusion of these features would create a more complicated model, adding realism but detracting from the current simple and transparent form.

The model currently simulates the ground combat on a 3 x 4 Km piece of coastal terrain representing an area of Ham-Hung, Korea. In order to simulate combat on a user's specific terrain, he needs to fit a parameterized terrain model to the actual terrain of interest. Doing so using the terrain fitting method described in the preceding chapter is an extremely tedious and time consuming process. The development of a more efficient terrain fitting technique will greatly enhance the model flexibility, and increase its utility in responding to interrogations from the real world.

The interested reader may obtain the model program deck and the sample input data deck from Prof. James G. Taylor, Naval Postgraduate School. Since the data used for the model run is hypothetical and greatly simplified, the reader is cautioned not to draw any analytical conclusions from the output.

APPENDIX A

SAMPLE EXPECTED OUTPUT

I. Amphibious Assault Summary

AMPHIBIOUS ASSAULT INFORMATION

INITIAL FORCE STRENGTH

| WAVE | 1 | 2 | 3 | 4 | 5 |
|------|------|------|------|------|-----|
| LVA | 10.0 | 11.0 | 11.0 | 10.0 | 3.0 |

DT = 3.0 DS = 1.0

LVA ENGR SPECS

| SPDMAX | SPDMIN | HTMAX | HTMIN | WID |
|--------|--------|-------|-------|------|
| 10.30 | 3.50 | 1.70 | 0.60 | 3.53 |

DEFENSIVE TACTICAL PARAMETERS

| | RANGE MAX | MIN | AIM-RELOAD TIME | PROJECTILE VELOCITY |
|------|--------------|-------|--------------------|------------------------|
| TANK | 1500.0 | | 15.00 | 350.00 |
| ATGM | 2000.0 | 200.0 | 30.00 | 350.00 |

DEFENSIVE TACTICAL ALLOCATION WEIGHTS:

WAVE 1 = 2.00 WAVE 2 = 1.00

DEFENSIVE FORCE ATTRITION COEFFICIENTS

| | ALPHA*A | BETA*A |
|----|---------|---------|
| DT | 0.00006 | 0.00070 |
| DS | 0.00008 | 0.00090 |

WBETA(1) = 0.00050 WBETA(2) = 0.00070

BREAKPOINT ASSUMPTION: 0.3*(TOTAL DEP FORCE)

DEFENSIVE FORCE LEVEL FOR GROUND ATK 0.32

DISPERSION DATA

| RANGE | TSIGV | RANGE | TSIGH | RANGE | TMEANH |
|---------|-------|---------|-------|---------|--------|
| 25.0 | 0.0 | 25.0 | 0.0 | 25.0 | 0.0 |
| 500.0 | 2.0 | 500.0 | 2.0 | 500.0 | 1.0 |
| 1000.0 | 5.0 | 1000.0 | 5.0 | 1000.0 | 5.0 |
| 2000.0 | 20.0 | 2000.0 | 20.0 | 2000.0 | 10.0 |
| 5000.0 | 25.0 | 5000.0 | 25.0 | 5000.0 | 15.0 |
| 10000.0 | 25.0 | 10000.0 | 25.0 | 10000.0 | 15.0 |

| RANGE | SSIGV | RANGE | SSIGH |
|---------|-------|---------|-------|
| 25.0 | 0.0 | 25.0 | 0.0 |
| 250.0 | 5.0 | 250.0 | 5.0 |
| 500.0 | 7.5 | 500.0 | 7.5 |
| 1000.0 | 14.0 | 1000.0 | 14.0 |
| 2500.0 | 15.5 | 2500.0 | 15.5 |
| 5000.0 | 17.0 | 5000.0 | 17.0 |
| 10000.0 | 20.0 | 10000.0 | 20.0 |

II. Assault Phase Time Step Summary

TIME = 815.0 SECONDS

| WAVE | FORCE LEVEL | STATUS | LOST-PCT | TSURV |
|---|-------------|--------|----------|-------|
| 1 | 0.7322 | 1 | 0.927 | |
| 2 | 1.7451 | 1 | 0.841 | |
| 3 | 4.5060 | 1 | 0.590 | |
| 4 | 9.8051 | 3 | 0.019 | |
| 5 | 3.0000 | 2 | 0.0 | |
| TANK | 0.0 | | 1.000 | 19.79 |
| ATGM | 0.0 | | 1.000 | 0.0 |
| FINAL LVA SURVIVORS ASHORE = | | | 19.788 | |
| GROUND ATTACK STARTS AFTER DEFENDER BROKE CONTACT | | | | |

GROUND ATK TIME = 825.0

III. Initial Ground Combat Summary

| INITIAL GROUND COMBAT INFORMATION | | | |
|-----------------------------------|--------|--------|-------------|
| UNIT | X | Y | FORCE LEVEL |
| 1 | 2000.0 | 1900.0 | 3.0 |
| 2 | 1900.0 | 2400.0 | 3.0 |
| 3 | 1500.0 | 2100.0 | 3.0 |
| 4 | 3800.0 | 2700.0 | 3.0 |
| 5 | 3800.0 | 2300.0 | 3.0 |
| 6 | 3600.0 | 1700.0 | 3.0 |

ATTRITION IS DETERMINISTIC

ROUTES DETERMINED BY USER

ATTACK VEHICLE SPEED IS 12.0

BREAKPOINT DISTANCE IS 500.0

DEFENDER WILL MOVE TO ALTERNATE POSITIONS
ALTERNATE POSITIONS ARE:

| UNIT | X | Y |
|------|--------|--------|
| 4 | 4500.0 | 3800.0 |
| 5 | 4500.0 | 2700.0 |
| 6 | 4600.0 | 1800.0 |

ATK KILL PROBABILITIES

| RANGE | P | PHH | PHM | PKH |
|-------|------|------|------|------|
| 500 | 0.85 | 0.85 | 0.75 | 0.70 |
| 1000 | 0.80 | 0.80 | 0.75 | 0.70 |
| 1500 | 0.75 | 0.75 | 0.70 | 0.65 |
| 2000 | 0.60 | 0.65 | 0.60 | 0.55 |
| 2500 | 0.45 | 0.50 | 0.50 | 0.35 |
| 3000 | 0.20 | 0.20 | 0.20 | 0.20 |

DEF. KILL PROBABILITIES

| RANGE | P | PHH | PHM | PKH |
|-------|------|------|------|------|
| 500 | 0.60 | 0.70 | 0.65 | 0.85 |
| 1000 | 0.85 | 0.90 | 0.85 | 0.90 |
| 1500 | 0.80 | 0.85 | 0.85 | 0.80 |
| 2000 | 0.75 | 0.80 | 0.75 | 0.70 |
| 2500 | 0.60 | 0.70 | 0.65 | 0.65 |
| 3000 | 0.40 | 0.45 | 0.40 | 0.50 |

IV. Ground Combat Time Step Summary

TIME = 1395 SECONDS

| UNIT | X | Y | FORCE LEVEL | STATUS | LOST-PCT | TARGETS |
|------|--------|--------|-------------|--------|----------|---------|
| 1 | 2420.8 | 1984.2 | 0.0 | 2 | 1.000 | |
| 2 | 3664.1 | 2253.0 | 0.0 | 2 | 1.000 | |
| 3 | 4397.4 | 1742.2 | 2.9 | 0 | 0.038 | |
| 4 | 4500.0 | 3800.0 | 0.0 | 2 | 1.000 | |
| 5 | 4500.0 | 2700.0 | 2.8 | 0 | 0.055 | |
| 6 | 4600.0 | 1800.0 | 0.0 | 2 | 1.000 | |

* DISTANCE BETWEEN FORCES IS TOO CLOSE. END OF BATTLE

APPENDIX B

LISTING OF SAMPLE INPUTS

I. Amphibious Assault Input

| | | | | | | |
|---------|---------|-------|-------|-------|--------|--------|
| 1 | 1 | | | | | |
| 10.30 | 3.5 | 1.7 | 0.6 | 3.533 | | |
| 10. | | | | | | |
| 1500. | 2000. | 200. | | | | |
| 15. | 30. | 350. | 350. | | | |
| 25. | 500. | 1000. | 2000. | 5000. | 10000. | 0. |
| 2. | 5. | 20. | 25. | 25. | | |
| 25. | 500. | 1000. | 2000. | 5000. | 10000. | 0. |
| 2. | 5. | 20. | 25. | 25. | | |
| 25. | 500. | 1000. | 2000. | 5000. | 10000. | 0. |
| 1. | 5. | 10. | 15. | 15. | | |
| 25. | 250. | 500. | 1000. | 2500. | 5000. | 10000. |
| 0. | 5. | 7.5 | 14. | 15.5 | 17. | 20. |
| 25. | 250. | 500. | 1000. | 2500. | 5000. | 10000. |
| 0. | 5. | 7.5 | 14. | 15.5 | 17. | 20. |
| 2. | 1. | | | | | |
| 10. | 11. | 11. | 10. | 3. | | |
| 3. | 1. | | | | | |
| 0.00006 | 0.00008 | | | | | |
| 0.0007 | 0.0009 | | | | | |
| 0.0005 | 0.0007 | | | | | |
| .32 | | | | | | |
| 50. | 100. | | | | | |

II. Terrain Data

| | | | | | |
|-------|-------|------|------|-------|-----|
| 46 | | | | | |
| 0. | | | | | |
| 2000. | 1100. | 170. | 0.1 | 999.9 | 8.0 |
| 1800. | 2200. | 150. | 30. | 350. | 2.0 |
| 2000. | 1900. | 150. | 130. | 300. | 2. |
| 2400. | 1400. | 150. | 0.1 | 300. | 2.5 |
| 2450. | 1700. | 130. | 80. | 500. | 2.2 |
| 2700. | 1800. | 138. | 90. | 500. | 2.2 |
| 3200. | 1650. | 140. | 150. | 600. | 3. |
| 4300. | 1300. | 130. | 160. | 400. | 3.5 |
| 3750. | 1750. | 150. | 0.1 | 660. | 3.6 |
| 4150. | 1600. | 150. | 160. | 550. | 3. |
| 3200. | 2150. | 130. | 25. | 500. | 1.5 |
| 4600. | 1700. | 170. | 45. | 300. | 2.5 |
| 4800. | 1500. | 170. | 0.1 | 300. | 2.5 |
| 2200. | 2600. | 170. | 90. | 350. | 1.8 |
| 2400. | 2850. | 150. | 120. | 300. | 1.8 |
| 3100. | 2700. | 150. | 150. | 350. | 2. |

| | | | | | |
|-------|-------|------|------|------|-----|
| 2500. | 2400. | 150. | 0.1 | 250. | 1.0 |
| 2650. | 2850. | 150. | 160. | 400. | 3.0 |
| 2700. | 2600. | 150. | 130. | 370. | 1.8 |
| 3800. | 2200. | 150. | 0.1 | 230. | 1.5 |
| 4500. | 2600. | 150. | 90. | 280. | 1.3 |
| 3600. | 2800. | 150. | 145. | 500. | 2.5 |
| 2700. | 3300. | 190. | 25. | 350. | 2.0 |
| 3000. | 3300. | 170. | 15. | 400. | 2.5 |
| 3150. | 3750. | 130. | 0.1 | 350. | 2.5 |
| 3750. | 3200. | 150. | 10. | 850. | 5.0 |
| 3800. | 3800. | 150. | 0.1 | 650. | 3. |
| 3600. | 3600. | 150. | 160. | 320. | 3.0 |
| 4150. | 3950. | 170. | 30. | 220. | 2.2 |
| 1650. | 2100. | 150. | 30. | 300. | 2.0 |
| 2250. | 2100. | 180. | 150. | 220. | 1.2 |
| 4000. | 2200. | 150. | 45. | 280. | 2. |
| 3900. | 2200. | 150. | 0.1 | 300. | 3.5 |
| 0 | 0 | 0 | 0 | 1 | 7 |
| 0 | 33 | 39 | 53 | 62 | 0 |
| 0 | 0 | 0 | 0 | 0 | 6 |
| 0 | 6 | 14 | 9 | 12 | 0 |
| 101 | | | | | |
| 1 | 2 | 3 | 30 | 4 | 43 |
| 6 | 32 | 33 | 7 | 11 | 31 |
| 8 | 9 | 10 | 11 | 33 | 43 |
| 8 | 42 | 2 | 14 | 30 | 23 |
| 16 | 17 | 18 | 19 | 20 | 3 |
| 2 | 31 | 11 | 16 | 20 | 22 |
| 46 | 20 | 21 | 22 | 12 | 34 |
| 42 | 45 | 46 | 14 | 23 | 15 |
| 26 | 14 | 25 | 26 | 27 | 28 |
| 35 | 44 | 26 | 27 | 29 | 35 |
| 40 | | | | | |

III. Ground Combat Input

```

1 28943
03 03
0000.0 2500.0 0500. 4000.0
3.0 3.0 3.0
1 2
2000.0 1900.0
1900.0 2400.0
1500.0 2100.0
01
5000.0 2500.0
01
4900.0 2150.0
02
2200.0 1700.0
4800.0 1750.0
3800.0 2700.0 3.0 190 120

```


| | | | | |
|--------|--------|------|------|-----|
| 3800.0 | 2300.0 | 3.0 | 190 | 120 |
| 3600.0 | 1700.0 | 3.0 | 180 | 120 |
| 0 | 0500.0 | 4 | | |
| 4500.0 | 3800.0 | | | |
| 4500.0 | 2700.0 | | | |
| 4600.0 | 1800.0 | | | |
| 0.85 | 0.85 | 0.75 | 0.70 | |
| 0.80 | 0.75 | 0.70 | 0.65 | |
| 0.75 | 0.75 | 0.70 | 0.65 | |
| 0.60 | 0.65 | 0.60 | 0.55 | |
| 0.45 | 0.50 | 0.50 | 0.35 | |
| 0.20 | 0.20 | 0.20 | 0.20 | |
| 0.60 | 0.70 | 0.65 | 0.85 | |
| 0.85 | 0.90 | 0.84 | 0.90 | |
| 0.80 | 0.85 | 0.85 | 0.80 | |
| 0.75 | 0.80 | 0.75 | 0.70 | |
| 0.60 | 0.70 | 0.65 | 0.65 | |
| 0.40 | 0.45 | 0.40 | 0.50 | |

APPENDIX C

DEFINITION OF VARIABLES IN COMPUTER PROGRAM

1. The Amphibious Assault Phase

CDSURV(I) = Current strength of defensive force I

I = 1 TANK

I = 2 ATGM

CSURV(I) = Current strength of assault wave I

DA(I) = Attrition rate for def. unit I due to the effects of ATFFS/TLF

DS1 = That portion of the DS unit assigned to engaging the closer of two multiple waves in the ATGM engagement window

DS2 = That portion of the Ds unit assigned to engaging the farther of two multiple waves in the ATGM engagement window

DT1 = That portion of the Dt unit assigned to engaging the closer of two multiple waves in the TANK engagement window

DT2 = That portion of the DT unit assigned to engaging the farther of two multiple waves in the TANK engagement window

DT1PH = Hit probability of rounds fired by DT1 against wave TENG(1)

DT1ROF = Rate of fire utilized by DT1 against wave TENG(1)

DINIT = Initial strength of def. force I

IL(I) = When equal to 1 indicates the wave landed shore

IWPN = Weapon code: TANK = 1, ATGM = 2

IWSTAT(I) = Current status of wave I

0 - not engaging

1 - landed

2 - under fire by ATGM

3 - under fire by TANK

4 - under fire both ATGM and TANK

GALF = Denote whether the LF build-up is sufficient
 for the ground attack
 0 - not sufficient
 1 - sufficient

GATK = Denote whether the LF initiated the ground attack
 0 - not started yet
 1 - started already

GATM = Time when the ground attack started

RD = Distance offshore at which waves initiate
 transition

RKSURV(I) = Concatenation of CSURV and CDSURV

SA(I) = Attrition rate for wave I due to ATGM

SENG(I) = The wave number of the closer of two waves in
 the ATGM engagement window

SRNG(I) = Firing range to wave SENG(I)

SSIGH = The std dev error in the horizontal for ATGM

SSIGV = The std dev error in the vertical for ATGM

SWTS(I) = The proportion of the total DS strength to be
 allowed to engaging SENG(I)

TA(I) = Attrition rate for wave I due to TANK

TBW = The interarrival time between waves arriving at
 the beach

TMEANH = The bias error in the horizontal for TANK

TMEANV = The bias error in the vertical for TANK

TENG(I) = The wave number of the closer of two waves in
 the tank engagement window

TRNG(I) = the firing range to wave TENG(I)

TSIGH = The std dev error in the horizontal for TANK

TSIGV = The std dev error in the vertical for TANK

TSURV = Total number of surviving LVA at the current time

TWTS(I) = The proportion of the total DT strength to be
 allowed to engaging TENG(I)

WVINT(I) = Initial strength of wave I

2. The Ground Attack Phase

| | | |
|-----------|---|--|
| ALPHA(I) | = | Initial attrition-rate coefficient for stochastic attrition module |
| APOA(I,J) | = | The average proportion of the j^{th} attacker of unit i allocated to fire on unit i |
| AVSP | = | Average speed of moving attacking units |
| BREAK | = | Breakpoint distance between attacking units and defenders |
| DISMAX | = | Maximum distance allowed between attacking units before the leading unit is delayed |
| DIST | = | The straight-line distance between two movement nodes inputed by the user |
| DST | = | The distance in meters to be moved each time step by attacking units |
| FL(I) | = | Force level of unit i |
| FO(I) | = | Force level of unit i |
| FO(I) | = | Initial force level of unit i |
| IALT | = | Denotes whether the user desires alternate defensive positions or not 0 - yes 1 - no |
| IC | = | Counts number of time units a defender has been moving |
| IDIR(I,J) | = | Direction of j^{th} interval in i^{th} route |
| II(I) | = | Interval index for unit i |
| IMOVE | = | Number of time units a defender is allowed for moving to an alternate position |
| IPRDIR(I) | = | Primary direction of movement for unit i |
| IRTE | = | Denotes whether user wants to input routes or not 0 - program determined routes 1 - user determined routes |
| IS | = | Random number seed used for stochastic attrition |
| ISECWD(I) | = | Width of search sector for unit i |

ISPD = Input variable to denote user's desired speed for attackers movement
1 - 9 mph
2 - 12 mph
3 - 15 mph
4 - 18 mph

ITEM = Input variable denoting number of time steps allowed for defender's move

ITIME = Current time, in seconds, of battle

ITRIT = Input variable denoting whether attrition will be stochastic or deterministic
0 - stochastic
1 - deterministic

IUSTAT(I) = Current status of unit i
0 - unit alive, not firing
1 - unit alive and firing
2 - unit killed
3 - unit moving

LOA(I,J) = The number of the j^{th} attacker of unit i

LOST(I,J) = Denotes whether line-of-sight exists between unit i and j or not

LOT(I,J) = The number of the j^{th} target of unit i

MVTDIR(I) = Movement direction of unit i

N(I) = Number of nodes inputed by user for route i

NA(I) = Number of attackers of unit i

NBU = Number of defense units

NF(I) = Number of time units i is allowed to fire at the same location

NLOSC(I,J) = Number of continuous time steps that line-of-sight does not exist between unit i and unit j

NOI(I) = Number of intervals in the i^{th} route

NRU = Number of attack units

NT(I) = Number of targets of unit i

OFL(I) = Force level of unit i during previous time step

| | |
|------------|--|
| $P(I,J)$ | = Probability of 1 st round hit by unit i in range band j |
| $PHH(I,J)$ | = Probability of a hit following a hit by unit i in range band j |
| $PHM(I,J)$ | = Probability of a hit following a miss by unit i in range band j |
| $PKH(I,J)$ | = Probability of a kill given a hit by unit i in range band j |
| PM | = The proportion of time a moving unit is searching for targets |
| $POA(I,J)$ | = The proportion of the j th attacker of unit i allocated to fire on unit i |
| $POL(I)$ | = Percent of unit i lost during the current time step |
| $PTT(I)$ | = Proportion of surviving firepower allocated to the i th target if there are j targets available |
| RANGE | = Current minimum distance between attackers and defenders |
| $Q(I,J)$ | = Probability that unit j is not detected by unit i at current time |
| RF | = Detection rate reduction factor for a firing unit (in comparison with non-firing unit) |
| RMINTK | = Minimum effective range for defending weapon system |
| RMINTW | = Minimum effective range for attacking weapon system |
| RMXTK | = Maximum effective range for defending weapon system |
| RMXTW | = Maximum effective range for attacking weapon system |
| $ROT(I,J)$ | = The range of the j th target of unit i |
| SIZETK | = Size of attacking vehicle |
| SIZETW | = Size of defending vehicle |
| $TA(K)$ | = Time to acquire a target for k th weapon system type (k = 1,2) |
| $TF1(K)$ | = Time of flight to 1000m for k th weapon system type (k = 1,2) |

TF2(K) = Time of flight to 2000m for k^{th} weapon system type ($k = 1,2$)
 TF3(K) = Time of flight to 3000m for k^{th} weapon system type ($k = 1,2$)
 TH(K) = Time to fire a round following a hit for weapon system type k ($k = 1,2$)
 TI(K) = Time to fire first round after target has been acquired for weapon system type k ($k = 1,2$)
 TM(K) = Time to fire a round following a miss for weapon system type k ($k = 1,2$)
 TNKFR = Firing rate for attacking weapon system
 TOWFR = Firing rate for defending weapon system
 TPOL(I) = Total percentage of lost since battle began for unit i
 VISFR(I,J) = The fraction of unit i seen by unit j
 VISFRA = Fraction of unit A as seen by unit B
 VISFRB = Fraction of unit B as seen by unit A
 X(I),Y(I) = Coordinates of unit i
 XA(I),YA(I) = Coordinates of alternate position for defender i
 XIC(I,J) = Coordinates of the j^{th} interval endpoint of the route for unit i
 YIC(I,J)
 XL,YL = Distance added to previous interval endpoint for vehicle to move DST during a time step
 XLOC(I,J) = Coordinates of the j^{th} node inputted by the user for the route of unit i
 YLOC(I,J)

APPENDIX D

PROGRAM LISTING

```

C  AMPHIBIOUS ASSAULT PHASE
COMMON /AMPH/ IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DIN,IT(2),GAINL,IMSTAT(5)
COMMON /ENGR/ SPDMAX,HTMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
COMMON /DISPER/TSIGV(6,2),TSGH(6,2),TMEANH(6,2),
1SSIGV(7,2),SSIGH(7,2)
COMMON /DEF/TENGMX,SENGMX,SENGMN,TARTM,SARTM,TVEL,
1SVEL,DEFWTS(2)
COMMON /SUPEFT/GAMMA,DELTA
COMMON /IOUT/ISURV,IATTR
C  GROUND ATTACK PHASE
COMMON /GRP1/ IPRDIR(6),ISECWD(6),MVTDIR(6),X(6),Y(6),SPD(6)
COMMON /GRP2/ TA(2),T1(2),TH(2),TF1(2),TF2(2),TF3(2),
1P(2,6),PHH(2,6),PHM(2,6),PKH(2,6),TF(2)
COMMON /GRP3/ NBU,NRU,FL(6),FO(6),NOI(3),XIC(3,200),YIC(3,200),
1IDIR(3,200),AVSP,ISPD
COMMON /GRP4/ VISFRA,VISFRB,SIZEK,
1IUSTAT(6),I1(6),LOST(6,6),DISMAX,
1SIZEK,NT(6),INF(6),SRF,DISMAX,
INLOSC(6,6),VISFR(6,6),RMINTK,RMINTW,RMXTW,OP,TOWFR,TNKFR,
1PTTT(3,3),RF,POA(6,6),APOA(6,6),LOA(6,6),NA(6,6),OFL(6),POL(6)
COMMON /GRP5/ TPOL(6),OLDQ(6,6),Q(6,6)
COMMON /HILLS/ LOT(6,6),ROT(6,6)
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ ECC(100),PXX(100),PXY(100),BASE
COMMON /HILLS/ NHILLS
COMMON /COVER/ CX(150),CPEAK(150),CPXX(150),CPYY(150)
COMMON /COVER/ CPXY(150),NCVELS
COMMON /COUNTR/ KH,KHW,KV,KN,KGRS,KELL,KINT
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(150),KTREP
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCREP(150)
COMMON /GRP6/ ALPHA(6)
COMMON /GRP7/ XA(6),YA(6),IMOVE(6)

GATM=0.
GATK=0.
CALL DATAIN
CALL SETUP
CALL SEA(GATM,GATK)
IF(GATK.NE.0.) GO TO 106
WRITE(6,105)
105 FORMAT(IX,'TOTAL LANDED LF STRENGTH IS NOT SUFFICIENT FOR GATK')

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106 STOP
107 IF(GATK-2.0) 10,20,30
108 WRITE(6,107)
109 FORMAT(IX,'GROUND ATTACK STARTS WHILE SHORE COMBAT IS GOING ON')
110 GO TO 110
111 GO TO 110
112 WRITE(6,108)
113 FORMAT(IX,'GROUND ATTACK STARTS AFTER DEFENDER BROKE CONTACT')
114 GO TO 110
115 GO TO 110
116 WRITE(6,109)
117 FORMAT(IX,'GROUND ATTACK STARTS AFTER ALL WAVES LANDED')
118 WRITE(6,111) GATM
119 FORMAT(IX,'GROUND ATK TIME=',F6.1)
120 CALL GROUND(GATM)
121 STOP
122 END

```

C

```

SUBROUTINE SEA(GATM,GATK)
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINIT(2),GAINL,IWSTAT(5)
COMMON /ENGR/ SPDMAX,SPDMIN,HTMAX,HTMIN,TTS,TAA,TB,TFF
CALL OUTPUT
IRD=500
ITBW=120
RD=1.0*IRD
TBW=1.0*ITBW
TINT=0.0

```

C

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COMPUTATION OF FIRST WAVE TIME PARAMETERS
TA-TIME FIRST WAVE INITIATES TRANSITION
TB-TIME FIRST WAVE COMPLETES TRANSITION
TFF-TIME FIRST WAVE REACHES THE BEACH

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C

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TAA=(5000.-RD)/SPDMAX
TB=TAA+TTS
TFF=TB+(RD-(0.5*(SPDMAX-SPDMIN)*TTS)-150.)/SPDMIN
DEL=10.
WRITE(6,55) RD,TBW
55 FORMAT(IX,'ITERATION INITIATED...RD=',F10.3,IX,'TBW=
1.,F10.3)
CALL RKINT(DEL,TINT,N,GATM,GATK)
RETURN
END
SUBROUTINE RKINT(H,TI,N,GATM,GATK)

```

C

```

SUBROUTINE RKINT PROVIDES THE INTERFACE BETWEEN
THE EULER NUMERICAL INTEGRATION ROUTINE(RKLEQ)
AND THE SUBROUTINE ATTR WHICH DETERMINES EACH
UNIT'S STATUS AS TIME PROGRESSES THROUGH THE

```

C


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C      AMPHIBIOUS OPERATION
C
      COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
      1TBW,DIN IT(2),GAINL,IWSTAT(5)
      COMMON /IOUT/ISURV,IATTR
      DIMENSION CSURV(5),CDSURV(2),TA(5),SA(5),DA(2)
      DIMENSION RKSURV(7),RKATTR(7),TATTR(200,12),TIME(200)

C      IMAX - MAXIMUM ALLOWABLE NUMBER OF TIME INTERVALS
C      ITE - A SWITCH VARIABLES SET TO 1 WHEN THE DEF.TANK
C           UNIT INITIATES ITS FIRE
C      ISE - A SWITCH VARIABLES SET TO 1 WHEN THE DEF.ATGM
C           UNIT INITIATES ITS FIRE
C      T - CURRENT TIME
C      IT - CURRENT TIME PERIOD
C
      GALF=0.
      IMAX=199
      ITE=0
      ISE=0
      TSURV=0.
      TIME(I)=0.
      T=TI
      DO 10 I=1,5
      CSURV(I)=WVINT(I)
      TSURV=TSURV+CSURV(I)
      IL(I)=0
      IWSTAT(I)=0
10     CONTINUE
      DO 15 I=1,2
      CDSURV(I)=DINIT(I)
15     CONTINUE
      DO 20 J=1,12
      TATTR(I,J)=0.
20     IT=1
      DO 25 I=1,5
      RKSURV(I)=CSURV(I)
25     RKSURV(6)=CSURV(1)
      RKSURV(7)=CSURV(2)
      DO 30 I=1,7
      RKATTR(I)=0.
30     NT=0
1000    CALL ATTR(T,CSURV,CDSURV,TA,SA,DA,GALF,GATK,GATM)
      IF(IL(1).EQ.99) GO TO 1200
      DO 40 I=1,5
      RKSURV(I)=CSURV(I)
40     RKATTR(I)={TA(I)+SA(I)}*(-1.0)
      DO 45 I=1,2

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GRA00900
GRA00910
GRA00920
GRA00930
GRA00940
GRA00950
GRA00960
GRA00970
GRA00980
GRA00990
GRA01000
GRA01010
GRA01020
GRA01030
GRA01040
GRA01050
GRA01060
GRA01070
GRA01080
GRA01090
GRA01100
GRA01110
GRA01120
GRA01130
GRA01140
GRA01150
GRA01160
GRA01170
GRA01180
GRA01190
GRA01200
GRA01210
GRA01220
GRA01230
GRA01240
GRA01250
GRA01260
GRA01270
GRA01280
GRA01290
GRA01300
GRA01310
GRA01320
GRA01330
GRA01340
GRA01350
GRA01360
GRA01370

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GRA01380
 GRA01390
 GRA01400
 GRA01410
 GRA01420
 GRA01430
 GRA01440
 GRA01450
 GRA01460
 GRA01470
 GRA01480
 GRA01490
 GRA01500
 GRA01510
 GRA01520
 GRA01530
 GRA01540
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 GRA01570
 GRA01580
 GRA01590
 GRA01600
 GRA01610
 GRA01620
 GRA01630
 GRA01640
 GRA01650
 GRA01660
 GRA01670
 GRA01680
 GRA01690
 GRA01700
 GRA01710
 GRA01720
 GRA01730
 GRA01740
 GRA01750
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 GRA01770
 GRA01780
 GRA01790
 GRA01800
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 GRA01830
 GRA01840
 GRA01850

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45  RKSURV(I+5)=CDSURV(I)
    RKATTR(I+5)=-1.0*DA(I)
    S=RKLEDEQ(7,RKSURV,RKATTR,T,H,NT)
    DO 50 I=1,5
      CSURV(I)=RKSURV(I)
    CONTINUE
    DO 55 I=1,2
      CDSURV(I)=RKSURV(I+5)
    CONTINUE
    IF(S-1.) 1100,1000,1200
1100 WRITE(6,60)
    60  FORMAT(IX,'ERRO..S.NE.1.OR.2')
    STOP
1200 CONTINUE
    IT=IT+1
    TSURV=0.
    DO 65 L=1,5
      TSURV=TSURV+CSURV(L)
    65  IF(TSURV.LE.0.) TSURV=0.
    TIME(IT)=T
    C PRINT RESULT OF SHIP TO SHORE MOVEMNET AFTER EACH TIME STEP
112  FORMAT(//IX,'TIME=',F6.1,IX,'SECONDS'//)
113  WRITE(6,113)
113  FORMAT(IX,'WAVE',2X,'FORCE LEVEL',2X,'STATUS',2X,'LOST-PCT',
113  12X,'TSURV')
    DO 66 I=1,4
      PLOST=1.-CSURV(I)/WVINT(I)
      WRITE(6,114) I,CSURV(I),IWSTAT(I),PLOST
114  FORMAT(3X,I1,3X,F10.4,5X,I1,5X,F8.3)
    66  CONTINUE
    PLOST=1.-CSURV(5)/WVINT(5)
    WRITE(6,115) CSURV(5),IWSTAT(5),PLOST,TSURV
115  FORMAT(3X,I5,3X,F10.4,5X,I1,5X,F8.3,2X,F5.2)
    PLOST=1.-CDSURV(1)/DINIT(1)
    WRITE(6,116) CDSURV(1),PLOST
116  FORMAT(IX,'TANK',2X,F10.4,11X,F8.3)
    PLOST=1.-CDSURV(2)/DINIT(2)
    TASURV=CDSURV(1)+CDSURV(2)
    WRITE(6,117) CDSURV(2),PLOST,TASURV
117  FORMAT(IX,'ATGM',2X,F10.4,11X,F8.3,2X,F5.2)
    C
    DO 80 J=1,5
      TATTR(IT,J)=TA(J)
    80  TATTR(IT,J+5)=SA(J)
    DO 85 J=1,2
      TATTR(IT,J+10)=DA(J)
    85  R=RNG(T-4.*TBW)
  
```


GRA01860
GRA01870
GRA01880
GRA01890
GRA01900
GRA01910
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GRA01950
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GRA01970
GRA01980
GRA01990
GRA02000
GRA02010
GRA02020
GRA02030
GRA02040
GRA02050
GRA02060
GRA02070
GRA02080
GRA02090
GRA02100
GRA02110
GRA02120
GRA02130
GRA02140
GRA02150
GRA02160
GRA02170
GRA02180
GRA02190
GRA02200
GRA02210
GRA02220
GRA02230
GRA02240
GRA02250
GRA02260
GRA02270
GRA02280
GRA02290
GRA02300
GRA02310
GRA02320
GRA02330

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C  DETERMINE IF ALL WAVES LANDED AND GROUND ATK STARTED
C  IF(R.LT.75.) GO TO 2000
    IF(IT.GT.IMAX) GO TO 2000
    IF(IL(1).EQ.99) GO TO 2000
    GO TO 1000
2000 N=IT
    WRITE(6,90) TSURV
    FORMAT(IX,F10.3)
    IF(GATK.GE.1.) GO TO 2222
    IF(TSURV.LT.9.) GO TO 2222
    GATK=3.
    GATM=T
    RETURN
2222
    FUNCTION RKLDEQ(N,Y,F,X,H,NT)
    DIMENSION Y(1),F(1),Q(25)
    NT=NT+1
    GO TO (1,2,3,4),NT
    1  H1=H
       AA=H1/4.0
       DO 11 J=1,N
       11 Q(J)=0.
       X=X+AA
       GO TO 5
       2  X=X+AA
       GO TO 5
       3  X=X+AA
       GO TO 5
       4  DO 93 L=1,N
       93 Y(L)=Y(L)+AA*F(L)
       NT=0
       X=X+AA
       RKLDEQ=2.
       GO TO 6
       5  DO 90 I=1,N
       90 Y(I)=Y(I)+AA*F(I)
       6  RETURN
    END

C  SUBROUTINE ATTR(T,CSURV,DSURV,TA,SA,DA,GALF,GATK,GATM)
C  GIVEN THE CURRENT TIME AND STATE VARIABLE STRENGTHS,
C  SUBROUTINE ATTR DETERMINES THE ATTRITION RATES AND UPDATES
C  THE STATUS OF EACH UNIT WITH RESPECT TO SHORE MOVEMENT
C  AND IMPLEMENTS THIS INFORMATION INTO THE ATTRITION LOSS RATE
C  COMPUTATION.

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C TA(I) - CURRENT ATTRITION LOSS RATE FOR WAVE I DUE TO TANK FIRE
C SA(I) - CURRENT ATTRITION LOSS RATE FOR WAVE I DUE TO ATGM FIRE
C DA(I) - CURRENT ATTRITION LOSS RATE FOR DEF. FORCE I DUE TO
C ATFFS(AMPHIBIOUS TASK FORCE FIRE SUPPORT)/TLF EFFECTS
C
C CCMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RO,WVINT(5),WID,
C 1TBW,DIN IT(2),GAINL,IWSTAT(5)
C CCMON /DEF/TENGMX,SENGMX,TARTM,SARTM,TVEL,
C 1SVEL,DEFWTS(2)
C INTEGER TENG(2),SENG(2)
C DIMENSION TRNG(2),TWTS(2),SRNG(2),DSURV(2),SWTS(2),
C 1CSURV(5),TA(5),SA(5),DA(5),DA(2)
C
C DO 10 I=1,5
C TA(I)=0.
C SA(I)=0.
C 10 CONTINUE
C
C DS1=0.
C DS2=0.
C DT1=0.
C DT2=0.
C FAC=1.0
C
C DETERMINE IF PART OF LANDING FORCE ADVANCE TO ATTACK INLAND
C KEY TERRAIN
C
C IF(GATK.EQ.1.0) GO TO 2929
C IF(GALF.EQ.1.0.AND.(DSURV(1)+DSURV(2)).LE.GAINL*(DINIT(1)
C 1+DINIT(2))) GATM=1
C IF(GALF.EQ.1.0.AND.(DSURV(1)+DSURV(2)).LE.GAINL*(DINIT(1)
C 1+DINIT(2))) GATK=1.0
C
C DETERMINE IF DEF. BREAKPOINT HAS BEEN REACHED
C
C 2929 IF((DSURV(1)+DSURV(2)).LT.0.3*(DINIT(1)+DINIT(2)))
C 1 GO TO 20
C
C DETERMINE ATTRITION RATE ON DEFENSIVE FORCES BY ATFFS
C BASED UPON AREA OR AIMED FIRE STATUS
C
C DA(1)=B(1)
C DA(2)=B(2)
C IF(ITE.EQ.0) DA(1)=A(1)*DSURV(1)
C IF(ISE.EQ.0) DA(2)=A(2)*DSURV(2)
C GO TO 30

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GRA02340
GRA02350
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GRA02370
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GRA02680
GRA02690
GRA02700
GRA02710
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GRA02730
GRA02740
GRA02750
GRA02760
GRA02770
GRA02780
GRA02790
GRA02800
GRA02810

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20 DSURV(1)=0.
   DSURV(2)=0.
   DA(1)=0.
   DA(2)=0.
   IF(GATK.EQ.1.) GO TO 3939
   GAT=1
C
C DETERMINE IF DEF.BREAKPOINT HAS BEEN REACHED BEFORE SUFFICIENT
C LANDING FORCE IS BUILT UP ON THE SHORE FOR INLAND ATTACK
C
97 DO 91 I=1,5
   WVRNG=RNG(GAT-TBW*(I-1))
   IF(WVRNG.LT.75.) IL(I)=1
   IF(IL(I).EQ.1) TLF=TLF+CSURV(I)
91 CONTINUE
   GAT=GAT+10.
   IF(TLF.LT.9.0.AND.IL(5).EQ.1) RETURN
   IF(TLF.LT.9.0.AND.IL(5).NE.1) GO TO 97
   GATK=2.
   GATF=1.
   GATM=GAT
   WRITE(6,220) GATM
220 FORMAT(7,1X,'GROUND ATK INITIATES AT TIME=',F7.1)
3939 IL(1)=99
25 WRITE(6,25) T
25 FORMAT(1X,'BEAKPOINT REACHED AT TIME = ',F9.3)
   RETURN
30 CALL DTGTS(T,TENG,TRNG,TWTS,SENG,SRNG,SWTS,CSURV)
C
C DETERMINE THE CUMULATIVE NUMBER OF SURVIVING LVA'S
C THAT HAVE BEEN REACHED THE BEACH - TLF
C
   TLF=0.
   DO 40 J=1,5
   IF(IL(J).EQ.1) TLF=TLF+CSURV(J)
40 CONTINUE
C
C DETERMINE IF TLF BUILT UP IS SUFFICIENT FOR GROUND ATK
C
   IF(TLF.GE.9.) GATF=1.
   IF(GATK.EQ.1.) TLF=TLF-9.
C
C ALLOCATE THE FORCE STRENGTH OF TLF BETWEEN THE TWO
C DEFENSIVE FORCE UNITS
C
   DSUM=DSURV(1)+DSURV(2)
   TLF1=(DSURV(1)/DSUM)*TLF
   TLF2=(DSURV(2)/DSUM)*TLF

```



```

C ADD TO DA1 AND DA2 THE ATTRITION LOSS RATE DUE
C TO THE EFFECTS OF TLF1 AND TLF2
C
C      DA{1}=DA{1}+TLF1*WB{1}
C      DA{2}=DA{2}+TLF2*WB{2}
C      IF(DSURV{1}.LE.0.0) DA{1}=0.0
C      IF(DSURV{2}.LE.0.0) DA{2}=0.0
C
C DETERMINE IF THERE EXISTS AN INCOMING WAVE IN THE
C TANK ENGAGEMENT WINDOW I.E. TENG(1).NE.0
C      IF(TENG(1).EQ.0.) GO TO 100
C      ITE=1
C
C DETERMINE THE TIME SINCE WAVE TENG(1) CROSSED THE
C 5000. METER OFFSHORE MARK -T1
C      T1=T-TBW*(TENG(1)-1)
C      DT1=TWTS(1)*DSURV(1)
C      FAC=1.
C
C DETERMINE THE SUPPRESSION EFFECT TO BE IMPOSED
C ON THE DT UNIT BASED ON THE ATTRITION LOSS RATE
C CURRENTLY IN EFFECT
C      SUPFAC=DA(1)
C
C      CALL RATE(TRNG(1),SPD(T1),1,SUPFAC,DT1ROF)
C      CALL PHIT(TRNG(1),WID,HT(T1),1,SUPFAC,DT1PH)
C
C DETERMINE THE ATTRITION LOSS RATE FOR WAVE TENG(1)
C DUE TO DT1 FIRES
C      TA(TENG(1))=DT1PH*DT1ROF*DT1
C
C DETERMINE IF THERE IS A SECOND INCOMING WAVE THAT
C IS IN THE TANK ENGAGEMENT WINDOW, IF THERE IS THE
C ATTRITION RATE COMPUTATIONS ARE SIMILAR IN FORM
C TC THOSE PREVIOUSLY PERFORMED FOR THE CLOSER WAVE
C
C      IF(TENG(2).EQ.0) GO TO 100
C      T2=T-TBW*(TENG(2)-1)
C      DT2=TWTS(2)*DSURV(1)
C      CALL RATE(TRNG(2),SPD(T2),1,SUPFAC,DT2ROF)
C      CALL PHIT(TRNG(2),WID,HT(T2),1,SUPFAC,DT2PH)
C      TA(TENG(2))=DT2PH*DT2ROF*DT2
C
C

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GRA03300
 GRA03310
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 GRA03590
 GRA03600
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 GRA03660
 GRA03670
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 GRA03690
 GRA03700
 GRA03710
 GRA03720
 GRA03730
 GRA03740
 GRA03750
 GRA03760
 GRA03770


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C C DETERMINE IF THERE EXISTS AN INCOMING WAVE IN THE ATGM
C C ENGAGEMENT WINDOW, IF THERE IS, DETERMINE THE ATTRITION
C C EFFECTS AGAINST THAT WAVE DUE TO ATGM THE ATTRITION
C C RATE COMPUTATION ARE SIMILAR IN FORM TO THOSE FOR THE
C C EFFECTS DUE TO THE TANK FIRE.
C C
100 IF(SENG(1).EQ.0) GO TO 200
   ISE=1
   SI=T-TBW*(SENG(1)-1)
   DS1=SWTS(1)*DSURV(2)
   SUPFAC=DA(2)
   CALL RATE(SRNG(1),SPD(S1),2,SUPFAC,DS1ROF)
   CALL PHIT(SRNG(1),WID,HT(T1),2,SUPFAC,DS1PH)
   SA(SENG(1))=DS1PH*DS1ROF*DS1
   IF(SENG(2).EQ.0) GO TO 200
   S2=T-TBW*(SENG(2)-1)
   DS2=SWTS(2)*DSURV(2)
   CALL RATE(SRNG(2),SPD(S2),1,SUPFAC,DS2ROF)
   CALL PHIT(SRNG(2),WID,HT(S2),2,SUPFAC,DS2PH)
   SA(SENG(2))=DS2PH*DS2ROF*DS2
200 RETURN
C C
C C SUBROUTINE DTGTS(T,TENG,TRNG,TWTS,SENG,SRNG,SWTS,CSURV)
C C
C C GIVEN THE CURRENT TIME AND LVA WAVE SURVIVOR POPULATIONS,
C C SUBROUTINE DTGTS DETERMINES THE WAVE NUMBERS THAT ARE
C C TO BE ENGAGED BY THE DT AND DS DEFENSIVE UNITS BASED
C C ON THE ENGAGEMENT WINDOW CRITERIA
C C
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINIT(2),GAINL,IWSTAT(5)
COMMON /DEF/TENGMX,SENGMX,SENGMN,TARTM,SARTM,TVEL,
1SVEL,DEFWTS(2)
INTEGER TENG(2),SENG(2)
DIMENSION TRNG(2),SRNG(2),TWTS(2),SWTS(2),CSURV(5),DEMO(5)
DO 10 I=1,2
  TENG(I)=0
  TWTS(I)=0
  TRNG(I)=0
  SRNG(I)=0
  SENG(I)=0
  SWTS(I)=0
10 CONTINUE
  JS=0
  JSUM=0.
  SSUM=0.

```

GRA03780
 GRA03790
 GRA03800
 GRA03810
 GRA03820
 GRA03830
 GRA03840
 GRA03850
 GRA03860
 GRA03870
 GRA03880
 GRA03890
 GRA03900
 GRA03910
 GRA03920
 GRA03930
 GRA03940
 GRA03950
 GRA03960
 GRA03970
 GRA03980
 GRA03990
 GRA04000
 GRA04010
 GRA04020
 GRA04030
 GRA04040
 GRA04050
 GRA04060
 GRA04070
 GRA04080
 GRA04090
 GRA04100
 GRA04110
 GRA04120
 GRA04130
 GRA04140
 GRA04150
 GRA04160
 GRA04170
 GRA04180
 GRA04190
 GRA04200
 GRA04210
 GRA04220
 GRA04230
 GRA04240
 GRA04250

RETURN
END

C

```

SUBROUTINE DATAIN
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINIT(2),GAINL,IWSTAT(5)
COMMON /ENGR/SPDMMAX,HTMAX,HTMIN,TTS,TAA,TB,TFF
COMMON /DISPER/TSIGV(6,2),TSIGH(6,2),TMEANH(6,2),
1SSIGV(7,2),SSIGH(7,2)
COMMON /DEF/TENGMX,SENGMX,SENGMN,TARTM,SARTM,TVEL,
1SVEL,DEFWTS(2)
COMMON /SUPEFT/GAMMA,DELTA
COMMON /IOUT/ISURV,IATTR
READ(5,50) ISURV,IATTR
READ(5,100) SPDMMAX,SPDMMIN,HTMAX,HTMIN,WID
READ(5,100) TTS
READ(5,100) TENGMX,SENGMX,SENGMN
READ(5,100) TARTM,SARTM,TVEL,SVEL
READ(5,100) ((TSIGV(I,J),I=1,6),J=1,2)
READ(5,100) ((TSIGH(I,J),I=1,6),J=1,2)
READ(5,100) ((TMEANH(I,J),I=1,6),J=1,2)
READ(5,100) ((SSIGV(I,J),I=1,7),J=1,2)
READ(5,100) ((SSIGH(I,J),I=1,7),J=1,2)
READ(5,100) (DEFWTS(I),I=1,2)
READ(5,103) (WVINT(I),I=1,5)
READ(5,100) (DINIT(I),I=1,2)
READ(5,101) (A(I),I=1,2)
READ(5,101) (B(I),I=1,2)
READ(5,101) (WB(I),I=1,2)
READ(5,110) GAINL
READ(5,101) GAMMA,DELTA
FORMAT(F5.2)
110 FORMAT(2I5)
150 FORMAT(7F10.3)
100 FORMAT(2F10.5)
101 FORMAT(5F10.5)
103 RETURN
END

```

110
150
100
101
103

C

```

SUBROUTINE OUTPUT
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINIT(2),GAINL,IWSTAT(5)
COMMON /DISPER/TSIGV(6,2),TSIGH(6,2),TMEANH(6,2),
1SSIGV(7,2),SSIGH(7,2)
COMMON /ENGR/SPDMMAX,HTMAX,HTMIN,TTS,TAA,TB,TFF
COMMON /DEF/TENGMX,SENGMX,SENGMN,TARTM,SARTM,TVEL,
1SVEL,DEFWTS(2)
COMMON /SUPEFT/GAMMA,DELTA

```

1

GRA04740
GRA04750
GRA04760
GRA04770
GRA04780
GRA04790
GRA04800
GRA04810
GRA04820
GRA04830
GRA04840
GRA04850
GRA04860
GRA04870
GRA04880
GRA04890
GRA04900
GRA04910
GRA04920
GRA04930
GRA04940
GRA04950
GRA04960
GRA04970
GRA04980
GRA04990
GRA05000
GRA05010
GRA05020
GRA05030
GRA05040
GRA05050
GRA05060
GRA05070
GRA05080
GRA05090
GRA05100
GRA05110
GRA05120
GRA05130
GRA05140
GRA05150
GRA05160
GRA05170
GRA05180
GRA05190
GRA05200
GRA05210

GRA05220
 GRA05230
 GRA05240
 GRA05250
 GRA05260
 GRA05270
 GRA05280
 GRA05290
 GRA05300
 GRA05310
 GRA05320
 GRA05330
 GRA05340
 GRA05350
 GRA05360
 GRA05370
 GRA05380
 GRA05390
 GRA05400
 GRA05410
 GRA05420
 GRA05430
 GRA05440
 GRA05450
 GRA05460
 GRA05470
 GRA05480
 GRA05490
 GRA05500
 GRA05510
 GRA05520
 GRA05530
 GRA05540
 GRA05550
 GRA05560
 GRA05570
 GRA05580
 GRA05590
 GRA05600
 GRA05610
 GRA05620
 GRA05630
 GRA05640
 GRA05650
 GRA05660
 GRA05670
 GRA05680
 GRA05690

```

C*** INPUT SUMMARY PRINTOUT
C
  20 WRITE(6,20)
    FORMAT(1,1X,'AMPHIBIOUS ASSAULT INFORMATION')
  22 WRITE(6,22)
    FORMAT(1X,'INITIAL FORCE STRENGTH')
  23 WRITE(6,23)
    FORMAT(1X,1,5X,'2',5X,'3',5X,'4',5X,'5')
  24 WRITE(6,24)
    FORMAT(1X,'LVA',5(2X,F4.1))
  21 WRITE(6,21)
    FORMAT(1X,'(DINIT',1,2)
    DT = 1X,F3.1,5X,'DS =',1X,F3.1)
  25 WRITE(6,25)
    FORMAT(1X,'LVA ENGR SPECS')
  26 WRITE(6,26)
    FORMAT(1X,'SPDMAX',2X,'SPDMIN',3X,'HTMAX',2X,'HTMIN',3X,'WID')
  27 WRITE(6,27)
    FORMAT(2X,F5.2,3X,F5.2,3X,F4.2,2X,F4.2)
  630 WRITE(6,630)
    FORMAT(1X,'DEFENSIVE TACTICAL PARAMETERS')
  631 WRITE(6,631)
    FORMAT(10X,'RANGE',4X,'AIM-RELOAD',3X,'PROJECTILE')
  632 WRITE(6,632)
    FORMAT(8X,'MAX',3X,'MIN',4X,'TIME',7X,'VELOCITY')
  633 WRITE(6,633)
    FORMAT(1X,'TANK',1X,F6.1,9X,F5.2,7X,F6.2)
  634 WRITE(6,634)
    FORMAT(1X,'ATGM',1X,F6.1,1X,F6.1,2X,F5.2,7X,F6.2)
  50 WRITE(6,50)
    DEFWTS(1),DEFWTS(2)
    1/,1X,'WAVE 1 =',F5.2,1X,'WAVE 2 =',F5.2)
  100 WRITE(6,100)
    DEFENSIVE FORCE ATTRITION COEFFICIENTS')
  101 WRITE(6,101)
    ALPHA*A',10X,'BETA*A')
  102 WRITE(6,102)
    A(1),B(1)
    FORMAT(1X,'DT',6X,F7.5,9X,F7.5)
  103 WRITE(6,103)
    A(2),B(2)
    FORMAT(1X,'DS',6X,F7.5,9X,F7.5)
  104 WRITE(6,104)
    WB(1),WB(2)
    FORMAT(1X,'WBETA(1) =',F7.5,1X,'WBETA(2) =',F7.5)
  105 WRITE(6,105)
    BREAKPOINT ASSUMPTION: 0.3*(TOTAL DEF FORCE))
  770 WRITE(6,770)
    GAINL
    DEFENDER ATTRITION LEVEL ALLOWING GROUND ATTACK',
    1/,1X,F5.2,*(TOTAL DEFENDER FORCE))
  771 WRITE(6,771)
    GAMMA,DELTA
  
```



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771 FORMAT(/IX,'ARTM SUP FACTOR=',F5.1,2X,'ERROR SUP FACTOR=',F5.1)
C*** DISPERSION DATA PRINTOUT
C
IDISP=1
IF (IDISP.EQ.0) RETURN
WRITE(6,601)
601 FORMAT(/IX,'DISPERSION DATA'//)
WRITE(6,602)
602 FORMAT(3X,'RANGE',2X,'TSIGV',2X,'RANGE',2X,'TSIGH',
12X,'RANGE',2X,'TMEANH')
DO 55 I=1,6
WRITE(6,603) TSIGV(I,1),TSIGV(I,2),TSIGH(I,1),TSIGH(I,2),
1TMEANH(I,1),TMEANH(I,2)
55 CONTINUE
603 FORMAT(1X,F7.1,2X,F5.1,1X,F7.1,1X,F5.1,1X,F7.1,1X,F5.1)
WRITE(6,604)
604 FORMAT(/3X,'RANGE',2X,'SSIGV',2X,'RANGE',2X,'SSIGH')
DO 56 I=1,7
WRITE(6,605) SSIGV(I,1),SSIGV(I,2),SSIGH(I,1),SSIGH(I,2)
56 CONTINUE
605 FORMAT(1X,F7.1,2X,F5.1,1X,F7.1,1X,F5.1)
WRITE(6,606)
606 FORMAT('1','THE AMPHIBIOUS ASSAULT PHASE BEGINS'///)
RETURN
END

C
SUBROUTINE PHIT(RANGE,W,H,IWPN,SUPFAC,PRHIT)
COMMON /AMPH/IL(5),WB(2),A(2),B(2),ITE,ISE,RD,WVINT(5),WID,
1TBW,DINIT(2),GAINL,IWSTAT(5)
COMMON /DISPER/TSIGV(6,2),TSIGH(6,2),TMEANH(6,2),
1SSIGV(7,2),SSIGH(7,2)
COMMON /SUPEFT/GAMMA,DELTA

C
PI=ARCCOS(-1.0)
IF(RANGE.LT.25.) STOP
IF(IWPN.EQ.1) GO TO 50
C ATGM FIRING DATA COMPUTATIONS
WMEANH=0.0
WMEANV=0.0
CALL INTRP(SSIGV,RANGE,WSIGV,7)
CALL INTRP(SSIGV,RANGE,WSIGV,7)
C TANK FIRING DATA COMPUTATIONS
50 WMEANH=0.0
CALL INTRP(TMEANH,RANGE,WMEANH,6)
CALL INTRP(TSIGV,RANGE,WSIGV,6)
CALL INTRP(TSIGH,RANGE,WSIGH,6)
C CONVERSION TO MILS

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```

100 Z=ARSIN(H/RANGE)
    WSIGV=WSIGV*(1.+DELTA*SUPFAC)
    WSIGH=WSIGH*(1.+DELTA*SUPFAC)
    TGTW=(Z*6400.0)/(2.0*PI)
    TGTW=(ARSIN(W/RANGE))*(6400.0/(2.0*PI))

C INSTITUTE NORMALITY ASSUMPTIONS TO CCMPUTE HORIZONTAL
C AND VERTICAL HIT PROBABILITIES
C
    C=-1.0*SQRT(1./2.)
    HOR1=((TGTW/2.)-WMEANH)/WSIGH
    HOR2=((-1.0*TGTW)/2.0)-WMEANH)/WSIGH
    PHITX=1.0
    IF(ABS(HOR1).GT.8.) GO TO 810
    PHITX=0.5*(ERFC(C*HOR1)-ERFC(C*HOR2))
810 VER1=((TGTW/2.)-WMEANH)/WSIGV
    VER2=((-1.0*TGTW)/2.)-WMEANH)/WSIGV
    PHITY=1.0
    IF(ABS(VER1).GT.8.) GO TO 820
    PHITY=0.5*(ERFC(C*VER1)-ERFC(C*VER2))
820 PRHIT=PHITX*PHITY
    RETURN
    END

C
C SUBROUTINE INTRP(X,ARG,VAL,N)
C DIMENSION X(N,2)
C WRITE(6,777) ARG
C 777 FORMAT(1X,'ARG**'= ,F10.3)
    IF(ARG.LT.X(1,1)) GO TO 500
    DO 50 I=1,N
    IF(ARG.GT.X(I+1,1)) GO TO 50
    DIFF=X(I+1,1)-X(I,1)
    DELTA=ARG-X(I,1)
    VAL=X(I,2)+(DELTA/DIFF)*(X(I+1,2)-X(I,2))
    RETURN
50 CONTINUE
    IF(ARG.GT.X(N,1)) GO TO 600
    VAL=X(N,2)
    RETURN
600 WRITE(6,601)
601 FORMAT(1X,'ERROR IN INTRP ARG.GT.X(N,2)')
    STOP
500 WRITE(6,501)
501 FORMAT(1X,'ERROR IN INTRP ARG.LT.X(1,1)')
    STOP
    END

C SUBROUTINE RATE(RANGE,SPEED,IWPN,SUPFAC,ROF)

```



```

COMMON /DEF/ TENG MX, SENG MX, SENG MN, TART M, SART M, TVEL, SVEL
COMMON /SUF/ FT/ GAM MA, DEL TA
ROF=0.0
IF(RANGE.LT.25.) RETURN
IF(IWPN.EQ.2) GO TO 500
IF(RANGE.GT.TENG MX) RETURN
TRTM=TART M*(1.0+GAM MA*SUF FAC)
DT=TRTM+RANGE/(TVEL+SPEED)
ROF=1.0/DT
RETURN
500 IF(RANGE.GT.SENG MX) RETURN
IF(RANGE.LT.SENG MN) RETURN
SRTM=SART M*(1.0+GAM MA*SUF FAC)
DT=SRTM+RANGE/(SVEL+SPEED)
ROF=1.0/DT
RETURN
END

C
FUNCTION SPD(T)
COMMON /ENGR/ SPD MAX, SPD MIN, HT MAX, HT MIN, TTS, TAA, TB, TFF
IF(T.GT.TAA) GO TO 50
SPD=SPD MAX
RETURN
50 IF(T.GT.TB) GO TO 100
SPD=SPD MIN+((TB-T)/TTS)*(SPD MAX-SPD MIN)
RETURN
100 SPD=SPD MIN
RETURN
END

C
FUNCTION HT(T)
COMMON /ENGR/ SPD MAX, SPD MIN, HT MAX, HT MIN, TTS, TAA, TB, TFF
IF(T.GT.TAA) GO TO 50
HT=HT MAX
RETURN
50 IF(T.GT.TB) GO TO 100
HT=HT MIN+((TB-T)/TTS)*(HT MAX-HT MIN)
RETURN
100 HT=HT MIN
RETURN
END

C
FUNCTION RNG(T)
COMMON /AMPH/ IL(5), WB(2), A(2), B(2), ITE, ISE, RD, WV INT(5), WID,
1TBW, DIN IT(2), GAIN L, IW STAT(5)
COMMON /ENGR/ SPD MAX, SPD MIN, HT MAX, HT MIN, TTS, TAA, TB, TFF
IF(T.GT.TAA) GO TO 50

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GRA06660
 GRA06670
 GRA06680
 GRA06690
 GRA06700
 GRA06710
 GRA06720
 GRA06730
 GRA06740
 GRA06750
 GRA06760
 GRA06770
 GRA06780
 GRA06790
 GRA06800
 GRA06810
 GRA06820
 GRA06830
 GRA06840
 GRA06850
 GRA06860
 GRA06870
 GRA06880
 GRA06890
 GRA06900
 GRA06910
 GRA06920
 GRA06930
 GRA06940
 GRA06950
 GRA06960
 GRA06970
 GRA06980
 GRA06990
 GRA07000
 GRA07010
 GRA07020
 GRA07030
 GRA07040
 GRA07050
 GRA07060
 GRA07070
 GRA07080
 GRA07090
 GRA07100
 GRA07110
 GRA07120
 GRA07130


```

RNG=5000.0-(SPDMA X*T)
RETURN
50 IF(T.GT.TB) GO TO 100
RNG=RD-0.5*(T-TAA)*(SPDMAX+SPD(T))
RETURN
100 IF(RNG=RD-((TB-TAA)/2.0)*(SPDMIN+SPDMAX))-((T-TB)*SPDMIN)
IF(RNG.LT.75.) RNG=0.0
RETURN
END

SUBROUTINE GROUND(GATM)
COMMON /GRP1/ IPRDIR(6), ISECWD(6), MVTDIR(6), X(6), Y(6), SPD(6)
COMMON /GRP2/ TA(2), TM(2), TF1(2), TF2(2), TF3(2),
1P(2,6), PHH(2,6), PHM(2,6), PKH(2,6), TF(2)
COMMON /GRP3/ NBU NRU, FL(6), FO(6), NOI(3), XIC(3,200), YIC(3,200),
1IDIR(3,200), AVSP, ISPD
1IUSTAT(6), II(6), LOST(6,6), VISFRA, VISFRB, SIZETK,
1SIZETW, NT(6), NF(6), SRF, DISMAX,
INLOSC(6,6), VISFR(6,6), RMINTK, RMXTK, RMINTW, RMXTW, OP, TOWFR, TNKFR,
1PTT(3,3), RF, POA(6,6), LQA(6,6), NA(6), OFL(6), POL(6)
COMMON /GRP4/ TPOL(6), OLDQ(6,6), Q(6,6)
COMMON /GRP5/ LOT(6,6), ROT(6,6)
COMMON /HILLS/ XC(100), PEAK(100), SX(100), SY(100), RHO(100)
COMMON /HILLS/ SCALE(100), TWORHO(100), TWOSCL(100), BASE
COMMON /HILLS/ NHILLS
COMMON /COVER/ CX(150), CPEAK(150), CPXX(150), CPYY(150)
COMMON /COVER/ CPXY(150), NCVELS
COMMON /COUNTR/ KH, KHW, KV, KN, KGRS, KELL, KINT
COMMON /GRID/ LST(10,10), NHL(10,10), LISTH(450), KHREP(100), KTREP
COMMON /GRID/ LSTC(10,10), NC(10,10), LISTC(400), KCREP(150)
COMMON /GRP6/ ALPHA(6)
COMMON /GRP7/ XA(6), YA(6), IMOVE(6)
INITIALIZATION.

BL=0.0
RL=0.0
MP=0
PAI=3.14159
ZL=.00001

READ TERRAIN DATA FOR LINE OF SIGHT
CHECK FOR STOCHASTIC OR DETERMINISTIC ATTRITION
ITRIT-ATTRITION MOD 1=DETERMINISTIC
0=STOCHASTIC
IS-SEED NUMBER

```

CC

CC

CC
CC
CC
CC
CC


```

130 READ(9,130) ITRIT,IS
   FORMAT(1,1X,I5)
   DO 132 I=1,6
   CALL LRND(1,IS,YRAN,1,1,0)
   ALPHA(1)=(-2.*YRAN**2)+(2.*YRAN+.3)
   WRITE(6,799) YRAN,ALPHA(1)
132 CONTINUE
799 FORMAT(2X,'YRAN,ALPHA',F10.5,2X,F10.5)
C
C READ IN NUMBER OF ATTACK AND DEFENSE UNITS
C
200 READ(9,200) NBU,NRU
   FORMAT(12,1X,I2)
C
C INITIALIZE WEAPON SIZES
C
   SIZETK=2.5
   SIZETW=2.5
C
C READ IN EFFECTIVE WEAPON RANGES
C
102 READ(9,102) RMINTK,RMXTK,RMINTW,RMXTW
   FORMAT(F6.1,1X,F6.1,1X,F6.1,1X,F6.1,1X)
C
C INITIALIZE PM,RF,TOWER,TNKFR AND NOD
C
   PM=.352
   RF=.5
   TOWER=.03
   TNKFR=.1
   NOD=2
   DO 101 I=1,NRU
   NOI(I)=125
101 CONTINUE
   K=NRU+1
   L=NRU+NBU
   DO 111 I=1,L
   II(I)=0
111 CONTINUE
C
C READ IN FORCE LEVELS OF EACH ATTACK UNIT
C
103 READ(9,103) (FL(I),I=1,NRU)
   FORMAT(3(F3.1,1X))
C
C CHECK FOR TYPE OF ROUTE DETERMINATION
C
   READ(9,106) IRTE,ISPD

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GRA07620
GRA07630
GRA07640
GRA07650
GRA07660
GRA07670
GRA07680
GRA07690
GRA07700
GRA07710
GRA07720
GRA07730
GRA07740
GRA07750
GRA07760
GRA07770
GRA07780
GRA07790
GRA07800
GRA07810
GRA07820
GRA07830
GRA07840
GRA07850
GRA07860
GRA07870
GRA07880
GRA07890
GRA07900
GRA07910
GRA07920
GRA07930
GRA07940
GRA07950
GRA07960
GRA07970
GRA07980
GRA07990
GRA08000
GRA08010
GRA08020
GRA08030
GRA08040
GRA08050
GRA08060
GRA08070
GRA08080
GRA08090

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GRA08100
GRA08110
GRA08120
GRA08130
GRA08140
GRA08150
GRA08160
GRA08170
GRA08180
GRA08190
GRA08200
GRA08210
GRA08220
GRA08230
GRA08240
GRA08250
GRA08260
GRA08270
GRA08280
GRA08290
GRA08300
GRA08310
GRA08320
GRA08330
GRA08340
GRA08350
GRA08360
GRA08370
GRA08380
GRA08390
GRA08400
GRA08410
GRA08420
GRA08430
GRA08440
GRA08450
GRA08460
GRA08470
GRA08480
GRA08490
GRA08500
GRA08510
GRA08520
GRA08530
GRA08540
GRA08550
GRA08560
GRA08570

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106 FORMAT(11,1X,11)
   IF(I SPD.EQ.1) AVSP=9.0
   IF(I SPD.EQ.1) DST=40.232
   IF(I SPD.EQ.2) AVSP=12.0
   IF(I SPD.EQ.2) DST=53.643
   IF(I SPD.EQ.3) AVSP=15.0
   IF(I SPD.EQ.3) DST=67.053
   IF(I SPD.EQ.4) AVSP=18.0
   IF(I SPD.EQ.4) DST=80.463
C
C READ IN INITIAL ATTACK UNIT'S LOCATIONS
C
      DC 6 I=1,NRU
      READ(9,107) XIC(I,1),YIC(I,1)
107 FORMAT(F6.1,1X,F6.1)
      6 CONTINUE
      IF(IRTE.EQ.1) GO TO 108
      DO 2 I=1,NRU
      DO 2 J=2,125
      YIC(I,J)=YIC(I,J-1)+DST*(J-1)
      XIC(I,J)=XIC(I,J-1)+DST*(J-1)
      IDIR(I,J)=0
      2 CONTINUE
      GO TO 109
108 CALL ROUTE
109 SUMRO=0.0
      DO 3 I=1,NRU
      FO(I)=FL(I)
      SUMRO=SUMRO+FO(I)
      X(I)=XIC(I,1)
      Y(I)=YIC(I,1)
      MVTDIR(I)=IDIR(I,1)
      SPD(I)=AVSP
      IUSTAT(I)=0
      IPRDIR(I)=IDIR(I,1)
      ISECWD(I)=120
      NF(I)=1
      IF(I)=1
      3 CONTINUE
C
C READ IN DEFENSE UNIT'S LOCATIONS
C
      SUMBO=0.0
      DO 4 I=K,L
      READ(9,104) X(I),Y(I),FL(I),IPRDIR(I),ISECWD(I)
104 FORMAT(F6.1,1X,F6.1,1X,F3.1,1X,I3,1X,I3)
      FO(I)=FL(I)
      SUMBO=SUMBO+FO(I)

```



```

MVTDIR(I)=0
SPD(I)=0.0
IUSTAT(I)=0
IMOVE(I)=0
4 CONTINUE

C CHECK FOR ALTERNATE DEFENSE POSITIONS AND READ IN IF WANTED
C
      READ(9,400) IALT, BREAK, ITEM
400  FORMAT(I1,1X,F6.1,1X,I2)
      IF(IALT.EQ.1) GO TO 401
      DO 402 I=K,L
402  READ(9,107) XA(I),YA(I)
401  CONTINUE
      TA(1)=20.
      TI(1)=8.
      TH(1)=8.
      TM(1)=10.
      TF1(1)=1.
      TF2(1)=1.
      TF3(1)=1.
      TA(2)=20.
      TI(2)=8.
      TH(2)=8.
      TM(2)=15.
      TF1(2)=10.
      TF2(2)=12.
      TF3(2)=15.

C READ IN HIT AND KILL PROBABILITIES
C
      DO 5 I=1,2
      DO 514 J=1,6
      READ(9,515) P(I,J),PHH(I,J),PHM(I,J),PKH(I,J)
515  FORMAT(4(F4.2,1X))
514  CONTINUE
      PTT(1,1)=1.0
      PTT(1,2)=0.8
      PTT(2,2)=0.2
      PTT(1,3)=0.8
      PTT(2,3)=0.15
      DC 31 I=1,NRU
      DO 31 I,J=K,L
      NLOSC(I,J)=0
      NLOSC(J,I)=0

```

```

GRA08580
GRA08590
GRA08600
GRA08610
GRA08620
GRA08630
GRA08640
GRA08650
GRA08660
GRA08670
GRA08680
GRA08690
GRA08700
GRA08710
GRA08720
GRA08730
GRA08740
GRA08750
GRA08760
GRA08770
GRA08780
GRA08790
GRA08800
GRA08810
GRA08820
GRA08830
GRA08840
GRA08850
GRA08860
GRA08870
GRA08880
GRA08890
GRA08900
GRA08910
GRA08920
GRA08930
GRA08940
GRA08950
GRA08960
GRA08970
GRA08980
GRA08990
GRA09000
GRA09010
GRA09020
GRA09030
GRA09040
GRA09050

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GRA09060
GRA09070
GRA09080
GRA09090
GRA09100
GRA09110
GRA09120
GRA09130
GRA09140
GRA09150
GRA09160
GRA09170
GRA09180
GRA09190
GRA09200
GRA09210
GRA09220
GRA09230
GRA09240
GRA09250
GRA09260
GRA09270
GRA09280
GRA09290
GRA09300
GRA09310
GRA09320
GRA09330
GRA09340
GRA09350
GRA09360
GRA09370
GRA09380
GRA09390
GRA09400
GRA09410
GRA09420
GRA09430
GRA09440
GRA09450
GRA09460
GRA09470
GRA09480
GRA09490
GRA09500
GRA09510
GRA09520
GRA09530

```

Q(I,J)=1.0
Q(J,I)=1.0
VISFR(I,J)=0.0
VISFR(J,I)=0.0
31 CONTINUE
IC=1

C PRINT INITIAL BATTLE INFORMATION
C
C
599 WRITE(6,599)
600 FORMAT(1,1X,'INITIAL GROUND COMBAT INFORMATION')
600 WRITE(6,600)
600 FORMAT(1X,'UNIT',7X,'X',8X,'Y',4X,'FORCE LEVEL')
DO 601 I=1,L
602 WRITE(6,602) I,X(I),Y(I),FL(I)
602 FORMAT(1X,I3,3X,F7.1,2X,F7.1,7X,F3.1)
601 CONTINUE
IF(I=IRIT.EQ.1) GO TO 603
WRITE(6,604)
604 FORMAT(1X,'ATTRITION IS STOCHASTIC')
GO TO 605
603 WRITE(6,606)
606 FORMAT(1X,'ATTRITION IS DETERMINISTIC')
606 IF(IRTE.EQ.0) GO TO 607
605 WRITE(6,608)
608 FCRMAT(1X,'ROUTES DETERMINED BY USER')
607 WRITE(6,609) AVSP
609 FORMAT(1X,'ATTACK VEHICLE SPEED IS ',F4.1)
610 WRITE(6,610) BREAK
610 FORMAT(1X,'BREAKPOINT DISTANCE IS ',F6.1)
IF(I=ALT.EQ.0) GO TO 615
WRITE(6,620)
620 FORMAT(1X,'DEFENDER WILL NOT MOVE TO ALTERNATE POSITIONS')
GO TO 625
615 WRITE(6,630)
630 FORMAT(1X,'DEFENDER WILL MOVE TO ALTERNATE POSITIONS',1X,
1,ALTERNATE POSITIONS ARE:',1X,'UNIT',5X,'X',8X,'Y')
DO 635 I=K,L
640 WRITE(6,640) I,XA(I),YA(I)
635 FORMAT(1X,I3,3X,F7.1,2X,F7.1)
635 CONTINUE
625 IRAN=500
645 WRITE(6,645)
645 FORMAT(1X,'ATK KILL PROBABILITIES',1X,'RANGE',4X,'P',
14X,'PHM',3X,'PHM',3X,'PKH')
DO 650 I=1,6
655 WRITE(6,655) IRAN,P(1,I),PHH(1,I),PHM(1,I),PKH(1,I)
655 FORMAT(2X,I4,4(2X,F4.2))

```


GRA09540
GRA09550
GRA09560
GRA09570
GRA09580
GRA09590
GRA09600
GRA09610
GRA09620
GRA09630
GRA09640
GRA09650
GRA09660
GRA09670
GRA09680
GRA09690
GRA09700
GRA09710
GRA09720
GRA09730
GRA09740
GRA09750
GRA09760
GRA09770
GRA09780
GRA09790
GRA09800
GRA09810
GRA09820
GRA09830
GRA09840
GRA09850
GRA09860
GRA09870
GRA09880
GRA09890
GRA09900
GRA09910
GRA09920
GRA09930
GRA09940
GRA09950
GRA09960
GRA09970
GRA09980
GRA09990
GRA10000
GRA10010

```

650  IRAN=IRAN+500
      CONTINUE
      WRITE(6,660)
660  FORMAT(/4X,'DEF. KILL PROBABILITIES'/1X,'RANGE',4X,'P',
14X,'PHH',3X,'PHM',3X,'PKH')
      DO 665 I=1,6
        WRITE(6,655) IRAN,P(2,I),PHH(2,I),PHM(2,I),PKH(2,I)
665  IRAN=IRAN+500
      CONTINUE
      WRITE(6,670)
670  FORMAT(11,10X,'BATTLE BEGINS',/)
      C  UPDATE LOCATION OF RED UNITS.
      DISMAX=5000.0
67  DO 9 I=1,NRU
      IF(IUSTAT(I).EQ.2) GOTO 9
      IF(IUSTAT(I).EQ.0) GOTO 76
      NF(I)=NF(I)+1
      IF(NF(I).LT.NOD) GOTO 9
      NF(I)=1
76  DO 11 J = 1, NRU
      IF (J.EQ.1) GO TO 11
      IF (IUSTAT(J).EQ.2) GO TO 11
      DIST = X(I) - X(J)
      IF (DIST.GT. DISMAX) GO TO 9
11  CONTINUE
      II(I) = II(I) + 1
      K7=II(I)
      X(I)=XIC(I,K7)
      Y(I)=YIC(I,K7)
      MVIDIR(I)=IDIR(I,K7)
      IPRDIR(I)=IDIR(I,K7)
      WRITE(6,666) I,X(I),Y(I),MVIDIR(I),IPRDIR(I)
      C 666 FORMAT(/,1X,I3,1X,F10.5,2X,F10.5,2X,I10,2X,I10,/)
      C 9 CONTINUE
      C  LINE--OF-SIGHT CHECK BETWEEN UNITS AND TARGETS SELECTION
      DO 17 J=K,L
      NT(J)=0
17  CONTINUE
      DO 12 I=1,NRU
      NT(I)=0
      IF(IUSTAT(I).EQ.2) GOTO 12
      DO 16 J=K,L
      IF(IUSTAT(J).EQ.2.OR.IUSTAT(J).EQ.3) GO TO 16
      XX1=X(I)

```


GRA10020
GRA10030
GRA10040
GRA10050
GRA10060
GRA10070
GRA10080
GRA10090
GRA10100
GRA10110
GRA10120
GRA10130
GRA10140
GRA10150
GRA10160
GRA10170
GRA10180
GRA10190
GRA10200
GRA10210
GRA10220
GRA10230
GRA10240
GRA10250
GRA10260
GRA10270
GRA10280
GRA10290
GRA10300
GRA10310
GRA10320
GRA10330
GRA10340
GRA10350
GRA10360
GRA10370
GRA10380
GRA10390
GRA10400
GRA10410
GRA10420
GRA10430
GRA10440
GRA10450
GRA10460
GRA10470
GRA10480
GRA10490

```

133 YY1=Y(I)
    CALL ELLEV(XX1,YY1,TMACI)
    XX2=X(J)
    YY2=Y(J)
    CALL ELLEV(XX2,YY2,TMACJ)
    LATOB=1
    LBTOA=1
    WRITE(6,675) XX1,YY1,TMACI,XX2,YY2,TMACJ
    FORMAT(IX,PRELOS,IX,6(F10.5,IX))
    CALL LOS(XX1,YY1,TMACI,0.0,SIZETK,XX2,YY2,TMACJ,0.0,SIZETW,
1  LATOB,LBTOA,VISFRA,VISFRB)
    VISFR(I,J)=VISFRA
    VISFR(J,I)=VISFRB
    IF(VISFRA.GT.ZL) GOTO 18
    LOST(I,J)=0
    LOST(J,I)=0
    NLOSC(I,J)=NLOSC(I,J)+1
    NLOSC(J,I)=NLOSC(I,J)
    GOTO 16
18  LOST(I,J)=1
    LOST(J,I)=1
    NLOSC(I,J)=0
    NLOSC(J,I)=0
    RANGE=SQRT((X(I)-X(J))**2+(Y(I)-Y(J))**2)
    IF(RANGE.LT.RMINTK.OR.RANGE.GT.RMXTK)GOTO 20
    IF(Q(I,J).EQ.1.0) GOTO 20
    IUSTAT(I)=1
    NT(I)=NT(I)+1
    M=NT(I)
    LOT(I,M)=J
    RCT(I,M)=RANGE
    IF(M.EQ.1) GOTO 20
    CALL SORT(I,M)
20  IF(RANGE.LT.RMINTW.OR.RANGE.GT.RMXTW) GOTO 16
    IF(Q(J,I).EQ.1.0) GOTO 16
    IUSTAT(J)=1
    NT(J)=NT(J)+1
    M=NT(J)
    LOT(J,M)=I
    RCT(J,M)=RANGE
    IF(M.EQ.1) GOTO 16
    CALL SORT(J,M)
16  CONTINUE
12  DO 25 I=1,NRU
    IF(IUSTAT(I).EQ.2) GOTO 25
    IF(NT(I).NE.0) GOTO 25
    IUSTAT(I)=0

```


GRA10980
GRA10990
GRA11000
GRA11010
GRA11020
GRA11030
GRA11040
GRA11050
GRA11060
GRA11070
GRA11080
GRA11090
GRA11100
GRA11110
GRA11120
GRA11130
GRA11140
GRA11150
GRA11160
GRA11170
GRA11180
GRA11190
GRA11200
GRA11210
GRA11220
GRA11230
GRA11240
GRA11250
GRA11260
GRA11270
GRA11280
GRA11290
GRA11300
GRA11310
GRA11320
GRA11330
GRA11340
GRA11350
GRA11360
GRA11370
GRA11380
GRA11390
GRA11400
GRA11410
GRA11420
GRA11430
GRA11440
GRA11450

```

IF(ANG.GT.AA) GOTO 24
PROP=PROP+PTT(I1,N5)
24 CONTINUE
IF(PROP.EQ.0.0) GOTO 34
IF(INT(J).GT.0)GOTO 36
CALL LAMDA(I,J,PCTVIS,DETRAT,PSUBK)
DETRAT=DETRAT*RF
QV=EXP(-(FL(I)*PROP*DETRAT*DELT*FL(J)))
Q(I,J)=Q(I,J)*QV
GOTO 19
36 Q(I,J)=0.0
GOTO 19
34 IF(IAA.EQ.1) GOTO 19
Q(I,J)=1.0
GOTO 19
15 IF(NLOSC(I,J).LE.3) GOTO 19
19 CONTINUE
14 CONTINUE
IF(IAA.EQ.K) GOTO 38
FR=TNKFR
IAA=K
IBB=L
ICC=1
IDD=NRU
OP=1.0
GOTO 37

FIRE ALLOCATION.

38 DO 28 I=1,L
28 NA(I)=0
DO 26 I=1,L
IF(IUSTAT(I).EQ.2.OR.IUSTAT(I).EQ.3) GO TO 26
IF(INT(I).EQ.0) GOTO 26
DC 27 J=1,3
APOA(I,J)=0.0
27 CONTINUE
IF(INT(I).EQ.1) GOTO 78
IF(INT(I).EQ.2) GOTO 79
NOT=3
MM1=LOT(I,1)
MM2=LOT(I,2)
MM3=LOT(I,3)
PROB=(1.0-Q(I,MM1))*Q(I,MM2)*Q(I,MM3)
APOA(I,1)=APOA(I,1)+PTT(I,1)*PROB
PROB=Q(I,MM1)*(1.0-Q(I,MM2))*Q(I,MM3)
APOA(I,2)=APOA(I,2)+PTT(I,1)*PROB

```

C
C
C

GRA11460
 GRA11470
 GRA11480
 GRA11490
 GRA11500
 GRA11510
 GRA11520
 GRA11530
 GRA11540
 GRA11550
 GRA11560
 GRA11570
 GRA11580
 GRA11590
 GRA11600
 GRA11610
 GRA11620
 GRA11630
 GRA11640
 GRA11650
 GRA11660
 GRA11670
 GRA11680
 GRA11690
 GRA11700
 GRA11710
 GRA11720
 GRA11730
 GRA11740
 GRA11750
 GRA11760
 GRA11770
 GRA11780
 GRA11790
 GRA11800
 GRA11810
 GRA11820
 GRA11830
 GRA11840
 GRA11850
 GRA11860
 GRA11870
 GRA11880
 GRA11890
 GRA11900
 GRA11910
 GRA11920
 GRA11930

```

PROB=Q(I,MM1)*Q(I,MM2)*(1.0-Q(I,MM3))
APOA(I,3)=APOA(I,1)+PTT(1,1)*PROB
PROB=(1.0-Q(I,MM1))*(1.0-Q(I,MM2))*Q(I,MM3)
APOA(I,1)=APOA(I,1)+PTT(1,2)*PROB
APOA(I,2)=APOA(I,2)+PTT(2,2)*PROB
PROB=(1.0-Q(I,MM1))*Q(I,MM2)*(1.0-Q(I,MM3))
APOA(I,1)=APOA(I,1)+PTT(1,2)*PROB
APOA(I,3)=APOA(I,3)+PTT(2,2)*PROB
PROB=Q(I,MM1)*(1.0-Q(I,MM2))*(1.0-Q(I,MM3))
APOA(I,2)=APOA(I,2)+PTT(1,2)*PROB
APOA(I,3)=APOA(I,3)+PTT(2,2)*PROB
PROB=(1.0-Q(I,MM1))*(1.0-Q(I,MM2))*(1.0-Q(I,MM3))
APOA(I,1)=APOA(I,1)+PTT(1,3)*PROB
APOA(I,2)=APOA(I,2)+PTT(2,3)*PROB
APOA(I,3)=APOA(I,3)+PTT(3,3)*PROB
DO 44 J=1,NOT
KK=LOT(I,J)
NA(KK)=NA(KK)+1
IN=NA(KK)
LOA(KK,IN)=I
POA(KK,IN)=APOA(I,J)
CONTINUE
44 GOTO 26
29 NOT=2
MM1=LOT(I,1)
MM2=LOT(I,2)
PROB=(1.0-Q(I,MM1))*Q(I,MM2)
APOA(I,1)=APOA(I,1)+PTT(1,1)*PROB
PROB=Q(I,MM1)*(1.0-Q(I,MM2))
APOA(I,2)=APOA(I,2)+PTT(1,1)*PROB
PROB=(1.0-Q(I,MM1))*Q(I,MM2)
APOA(I,1)=APOA(I,1)+PTT(1,2)*PROB
APOA(I,2)=APOA(I,2)+PTT(2,2)*PROB
GOTO 30
78 NOT=1
MM1=LOT(I,1)
PROB=1.0-Q(I,MM1)
APOA(I,1)=APOA(I,1)+PTT(1,1)*PROB
GOTO 30
26 CONTINUE
ATTRITION.
SUMR=0.0
SUMB=0.0
DO 40 I=1,L
IF(IUSTAT(I).EQ.2.OR.IUSTAT(I).EQ.3) GO TO 40
  
```

C
 C
 C


```

M6=NA(I)
SUM=0.0
IF(M6.EQ.0) GOTO 47
DO 41 J=1,M6
M7=LOA(I,J)
IF(M7.LT.K) GOTO 42
I TYPE=2
GOTO 43
42 I TYPE=1
43 RANGE=SQR T((X(I)-X(M7))**2+(Y(I)-Y(M7))**2)
IF (I TRIT.EQ.1) GO TO 131
CALL STOCH(I TYPE,RANGE,AJI)
GO TO 5000
131 CALL ET K(I TYPE,RANGE,T)
AJI=1.0/T
SUM=SUM+AJI*FL(M7)*POA(I,J)*DEL T
CONTINUE
41 OFL(I)=FL(I)
47 FL(I)=FL(I)-SUM
IF(FL(I).GT.ZL) GOTO 46
FL(I)=0.0
IUSTAT(I)=2
IF(I.LT.K) GOTO 60
SUMB=SUMB+FL(I)
TPOL(I)=(FO(I)-FL(I))/FO(I)
GO TO 40
60 SUMR=SUMR+FL(I)
TPOL(I)=(FO(I)-FL(I))/FO(I)
40 CONTINUE

PRINT AND CHECK FOR BATILE DETERMINATION.

C
C
C
C
I TIME=IC*10
DO 57 I=K,L
IF(IUSTAT(I).EQ.2) GO TO 57
DO 58 J=1,NRU
IF(IUSTAT(J).EQ.2) GO TO 58
CHECK=X(I)-X(J)
AVD=SQR T((X(I)-X(J))**2+(Y(I)-Y(J))**2)
IF(AVD.LT.BREAK.OR.CHECK.LT.50.) GO TO 250
58 CONTINUE
57 GO TO 99

C
C
C
C
COMPLETE ATTACK UNIT'S MOVE
250 DO 251 I=K,L

```


GRA12420
GRA12430
GRA12440
GRA12450
GRA12460
GRA12470
GRA12480
GRA12490
GRA12500
GRA12510
GRA12520
GRA12530
GRA12540
GRA12550
GRA12560
GRA12570
GRA12580
GRA12590
GRA12600
GRA12610
GRA12620
GRA12630
GRA12640
GRA12650
GRA12660
GRA12670
GRA12680
GRA12690
GRA12700
GRA12710
GRA12720
GRA12730
GRA12740
GRA12750
GRA12760
GRA12770
GRA12780
GRA12790
GRA12800
GRA12810
GRA12820
GRA12830
GRA12840
GRA12850
GRA12860
GRA12870
GRA12880
GRA12890

```

IF(IALT.EQ.1.OR.IMOVE(I).EQ.ITEM) GO TO 6000
IF(IUSTAT(I).EQ.0) IUSTAT(I)=3
IMOVE(I)=IMOVE(I)+1
IF(IMOVE(I).LT.ITEM) GO TO 251
X(I)=XA(I)
Y(I)=YA(I)
IF(IUSTAT(I).EQ.3) IUSTAT(I)=0
251 CONTINUE
99 IITIME=IITIME+IFIX(GATM)
WRITE(6,112) IITIME
112 FORMAT(//1X,'TIME=',I4,1X,'SECONDS'//)
113 WRITE(6,113)
113 FORMAT(1X,'UNIT',5X,'X',8X,'Y',5X,'FORCE LEVEL',2X,'STATUS',
12X,'LOST-PCT',2X,'TARGETS')
DO 59 I=1,L
N6=NT(I)
IF(N6.NE.0) GO TO 48
WRITE(6,264) I,X(I),Y(I),FL(I),IUSTAT(I),TPOL(I)
264 FORMAT(3X,I1,3X,F7.1,2X,F7.1,6X,F3.1,9X,I1,6X,F5.3)
GO TO 59
48 WRITE(6,114) I,X(I),Y(I),FL(I),IUSTAT(I),TPOL(I),
1(LOT(I),J),J=1,N6)
114 FORMAT(3X,I1,3X,F7.1,2X,F7.1,6X,F3.1,9X,I1,6X,F5.3,3X,I1,1X)
59 CONTINUE
C
C CHECK FOR BATTLE TERMINATION.
C
IOT=0
DO 53 I=1,NRU
IF(FL(I).EQ.0.0) GOTO 53
IOT=1
53 CONTINUE
IF(IOT.EQ.1) GOTO 54
WRITE(6,117)
117 FORMAT(1X,'*ATTACK FORCE IS ELIMINATED. END OF BATTLE.')
54 GOTO 66
IOT=0
DO 55 I=K,L
IF(FL(I).EQ.0.0) GOTO 55
IOT=1
55 CONTINUE
IF(IOT.EQ.1) GOTO 65
WRITE(6,118)
118 FORMAT(1X,'*DEFENSE FORCE IS ELIMINATED. END OF BATTLE.')
6000 WRITE(6,119)
119 FORMAT(1X,'*DISTANCE BETWEEN FORCES IS TOO CLOSE. END OF BATTLE
1.)

```


GRA12900
 GRA12910
 GRA12920
 GRA12930
 GRA12940
 GRA12950
 GRA12960
 GRA12970
 GRA12980
 GRA12990
 GRA13000
 GRA13010
 GRA13020
 GRA13030
 GRA13040
 GRA13050
 GRA13060
 GRA13070
 GRA13080
 GRA13090
 GRA13100
 GRA13110
 GRA13120
 GRA13130
 GRA13140
 GRA13150
 GRA13160
 GRA13170
 GRA13180
 GRA13190
 GRA13200
 GRA13210
 GRA13220
 GRA13230
 GRA13240
 GRA13250
 GRA13260
 GRA13270
 GRA13280
 GRA13290
 GRA13300
 GRA13310
 GRA13320
 GRA13330
 GRA13340
 GRA13350
 GRA13360
 GRA13370

```

65 GO TO 66
66 IC=IC+1
67 GO TO 67
68 RETURN
69 END

C SUBROUTINE SETUP
C SUBROUTINE SETUP IS USED TO READ IN THE TERRAIN DATA AND
C CREATE PARAMETRIC TERRAIN. THIS TERRAIN DATA WILL BE USED
C WHEN COMPUTING LINE-OF-SIGHT BETWEEN TARGETS AND OBSERVERS
C AS WELL AS PROVIDING A GRID SYSTEM FOR UNIT LOCATIONS AND
C MOVEMENT.

COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ ECC(100),PXX(100),PY(100),PXY(100),BASE
COMMON /HILLS/ NHILLS
COMMON /COVER/ CX(150),CY(150),CPEAK(150),CPXX(150),CPYY(150)
COMMON /COVER/ CPXY(150),NCVELS
COMMON /COUNTR/KH,KHW,KV,KN,KGRS,KELL,KINT
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(150),KTREP
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCREP(150)
PAI=3.14159
L=5
READ(L,7) NHILLS
READ(L,47) BASE
FORMAT(10.4)
FORMAT(16)
FORMAT(6F10.3)
DO 50 I=1,NHILLS
  READ(L,17) XC(I),YC(I),PEAK(I),ANGH(I),SPRD(I),ECC(I)
CONTINUE
READ(L,37) LST
READ(L,37) NHL
READ(L,7) NHTOT
READ(L,37) (LISTH(I),I=1,NHTOT)
FORMAT(10I5)
DO 100 I=1,NHILLS
  AANGLE=ANGH(I)*PAI/180.
  SANG=SIN(AANGLE)
  CANG=COS(AANGLE)
  A=PEAK(I)/(PEAK(I)-50.)
  A=ALOG(A)
  B=A*ECC(I)**2
  SSPD=SPRD(I)**2
  PXX(I)=-(A*CANG*CANG+B*SANG*SANG)/SSPD
  PYY(I)=-(A*SANG*SANG+B*CANG*CANG)/SSPD
  PXY(I)=(2.*SANG*CANG*(B-A))/SSPD
  KHREP(I)=-2147483600
  
```

C
 C
 C
 C
 C
 C

47
 7
 17
 50
 37

65

GRA13380
GRA13390
GRA13400
GRA13410
GRA13420
GRA13430
GRA13440
GRA13450
GRA13460
GRA13470
GRA13480
GRA13490
GRA13500
GRA13510
GRA13520
GRA13530
GRA13540
GRA13550
GRA13560
GRA13570
GRA13580
GRA13590
GRA13600
GRA13610
GRA13620
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GRA13640
GRA13650
GRA13660
GRA13670
GRA13680
GRA13690
GRA13700
GRA13710
GRA13720
GRA13730
GRA13740
GRA13750
GRA13760
GRA13770
GRA13780
GRA13790
GRA13800
GRA13810
GRA13820
GRA13830
GRA13840
GRA13850

```

C  ALL VALUES NOW IN METERS ON 0 -- 10,000 GRID
100  CONTINUE
    READ(L,7) NCVELS
    IF(NCVELS.EQ.0) GO TO 75
    DO 60 I=1,NCVELS
      READ(L,27) CXC(I),CYC(I),CPEAK(I),CPXX(I),CPYY(I),CPXY(I)
      FORMAT(3F10.4,3E13.7)
      KCREP(I)=-2147483600
    CONTINUE
    READ(L,37) LSTC
    READ(L,37) INC
    READ(L,7) NCTOT
    READ(L,37) (LISTC(I),I=1,NCTOT)
75  KTRIP=-2147483600
    KH=0
    KHW=0
    KV=0
    KN=0
    KGRS=0
    KELL=0
    KINT=0
    RETURN
    END

C  SUBROUTINE ROUTE
C  SUBROUTINE ROUTE COMPUTES THE ROUTE OF EACH ATTACKING UNIT
C  WHEN THE USER HAS SELECTED THE OPTION OF INPUTTING ATTACKER UNIT
C  ROUTES. IT CALCULATES THE COORDINATES OF EACH INTERVAL ENDPOINT
C  ALONG THE ROUTE, MAKING EACH INTERVAL LENGTH(DISTANCE MOVED DURING
C  A 10 SECOND TIME STEP) THE SAME. THE INTERVAL LENGTH IS DETERMINED
C  BY THE SPEED THE USER HAS SELECTED AND INPUTED FOR THE CURRENT
C  BATTLE.
C  COMMON /GRP3/ NBU,NRU,FL(6),F0(6),NOI(3),XIC(3,200),YIC(3,200),
1  IDIR(3,200),AVSP,ISPD
1  IJUSTAT(6),I(6),LOST(6,6),VISFRA,VISFRB,SIZEK,
1  ISIZETW,NT(6),NF(6),SRF,DISMAX,
1  INLOSC(6,6),VISFR(6,6),RMINTK,RMXTK,RMINTW,RMXTW,OP,TOWER,TNKFR,
1  IPTT(3,3),RF,POA(6,6),APOA(6,6),LOA(6,6),OFL(6),POL(6)
C  DIMENSION XLOC(3,20),YLOC(3,20),N(3)
C  IF(ISPD.EQ.4) DST=80.463
C  IF(ISPD.EQ.3) DST=67.053
C  IF(ISPD.EQ.2) DST=53.643
C  IF(ISPD.EQ.1) DST=40.232
C  LN=9
C  DO 300 I=1,NRU
    READ(LN,15) N(I)

```


GRAL3860
 GRAL3870
 GRAL3880
 GRAL3890
 GRAL3900
 GRAL3910
 GRAL3920
 GRAL3930
 GRAL3940
 GRAL3950
 GRAL3960
 GRAL3970
 GRAL3980
 GRAL3990
 GRAL4000
 GRAL4010
 GRAL4020
 GRAL4030
 GRAL4040
 GRAL4050
 GRAL4060
 GRAL4070
 GRAL4080
 GRAL4090
 GRAL4100
 GRAL4110
 GRAL4120
 GRAL4130
 GRAL4140
 GRAL4150
 GRAL4160
 GRAL4170
 GRAL4180
 GRAL4190
 GRAL4200
 GRAL4210
 GRAL4220
 GRAL4230
 GRAL4240
 GRAL4250
 GRAL4260
 GRAL4270
 GRAL4280
 GRAL4290
 GRAL4300
 GRAL4310
 GRAL4320
 GRAL4330

```

15  FORMAT(I2)
    NL=N(I)+1
    DO 200 IN=2,NL
      READ(LN,201) XLNCS,YLCS
201  FORMAT(F6.1,1X,F6.1)
      XLOC(I,IN)=XLNCS
      YLOC(I,IN)=YLCS
200  CONTINUE
      XLOC(I,1)=XIC(I,1)
      YLOC(I,1)=YIC(I,1)
      IDIR(I,1)=0
      NL=N(I)
      NUM=2
      DO 305 J=1,NL
        XL=XLOC(I,J+1)-XLOC(I,J)
        YL=YLOC(I,J+1)-YLOC(I,J)
        DIST=SQRT{XL**2+YL**2}
        Y=ABS(YL)
        Z=Y/XL
        ANGL=ATAN(Z)
        DEG=ANGL*57.2958
        IF(J.EQ.1) GO TO 320
        XLN=(DIST-EXTRA)*COS(ANGL)
        YLN=(DIST-EXTRA)*SIN(ANGL)
        XIC(I,NUM)=XIC(I,NUM-1)+XLN+XLE
        IF(YL.GT.0.) GO TO 325
        YLN=-YLN
325  YIC(I,NUM)=YIC(I,NUM-1)+YLN+YLE
        IF(YL.GT.0.) GO TO 340
        IDIR(I,NUM)=-IFIX(DEG)
        GO TO 341
        IDIR(I,NUM)=IFIX(DEG)
340  NUM=NUM+1
341  XLN=DST*COS(ANGL)
320  YLN=DST*SIN(ANGL)
        IF(YL.GT.0.) GO TO 310
        YLN=-YLN
310  IF(DIST.LT.DST) GO TO 315
        XIC(I,NUM)=XIC(I,NUM-1)+XLN
        YIC(I,NUM)=YIC(I,NUM-1)+YLN
        IF(YL.GT.0.) GO TO 342
        IDIR(I,NUM)=-IFIX(DEG)
        GO TO 343
        IDIR(I,NUM)=IFIX(DEG)
342  DIST=DIST-DST
343  NUM=NUM+1
        GO TO 310
  
```



```

315 EXTRA=DIST
XLE=EXTRA*COS(ANGL)
YLE=EXTRA*SIN(ANGL)
IF(YL.GT.0.) GO TO 305
YLE=-YLE
305 CONTINUE
300 CONTINUE
RETURN
END
C
C SUBROUTINE LAMDA(I,J,PCIVIS,DETRAT,PK)
C
C SUBROUTINE LAMDA IN CONJUNCTION WITH THE LOS ROUTINE COMPUTES
C THE DETECTION RATE(DETRAT) OF TARGET J BY THE OBSERVER I GIVEN
C THE PERCENT OF TARGET VISIBLE (PCIVIS) TO THE OBSERVER.
C
C COMMON /GRP1/ IPRDIR(6), ISECWD(6), MVTDIR(6), X(6), Y(6), SPD(6)
TCFACT=1.0
ZEROL=0.00001
PAI=3.14159
D=(ISECWD(I)*PAI/180.0)/2.0
BBB=(1.0/(2.0*(SIN(D)-D*COS(D))))
IF(ABS(BBB).LT.ZEROL) BBB=0.0
AAA=(-BBB)*COS(D)
IF(ABS(AAA).LT.ZEROL) AAA=0.0
OTANG=ATAN2((Y(J)-Y(I)),(X(J)-X(I)))
IF(OTANG.LT.-PAI/2.AND.OTANG.GT.-PAI) OTANG=2*PAI+OTANG
PD=IPRDIR(I)*PAI/180.0
IF((PD*OTANG).GE.0.0) GOTO 1
IF(PD.LT.0.0) GOTO 9
ANGLE=2*PAI+OTANG-PD
GOTO 10
9 ANGLE=2*PAI+PD-OTANG
10 IF(ANGLE.GT.PAI) ANGLE=2*PAI-ANGLE
1 GOTO 2
2 IF(ANGLE.GT.0) GOTO 3
DUP=PD+D
DLOW=PD-D
ANGLFT=OTANG+(15.0*PAI/180.)
IF(ANGLFT.GT.DUP) ANGLFT=DUP
ANGLRT=OTANG-(15.0*PAI/180.)
IF(ANGLRT.LT.DLOW) ANGLRT=DLOW
PK=BBB*ABS(ABS(SIN(ANGLFT))-ABS(SIN(ANGLRT)))+AAA*(ANGLFT-
1 ANGLRT)
IF(PK.LT.0.0) GOTO 3
IF(PK.GT.1.0) GOTO 5
GOTO 8

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GRA14340
 GRA14350
 GRA14360
 GRA14370
 GRA14380
 GRA14390
 GRA14400
 GRA14410
 GRA14420
 GRA14430
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 GRA14450
 GRA14460
 GRA14470
 GRA14480
 GRA14490
 GRA14500
 GRA14510
 GRA14520
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 GRA14550
 GRA14560
 GRA14570
 GRA14580
 GRA14590
 GRA14600
 GRA14610
 GRA14620
 GRA14630
 GRA14640
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 GRA14670
 GRA14680
 GRA14690
 GRA14700
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 GRA14790
 GRA14800
 GRA14810

GRA14820
 GRA14830
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 GRA14900
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 GRA14990
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 GRA15140
 GRA15150
 GRA15160
 GRA15170
 GRA15180
 GRA15190
 GRA15200
 GRA15210
 GRA15220
 GRA15230
 GRA15240
 GRA15250
 GRA15260
 GRA15270
 GRA15280
 GRA15290

```

3  PK=0.0
   DETRAT=0.0
   GOTO 6
5  GK=1.0
8  RANGE=SQRT((X(J)-X(I))**2+(Y(J)-Y(I))**2)
   RR=0.001*RANGE/PCTVIS
   TOANG=ATAN2((Y(I)-Y(J)),(X(I)-X(J)))
   AD=MVTDIR(J)*PAI/180.0
   HORVEL=ABS(SPD(J)*SIN(TOANG-AD))
   HCRVEL=HORVEL*1609.3/3600.0
   DENOM=1.453+TCFACT*(0.5978+2.188*(RR**2)-0.5038*HORVEL)
   IF(DENOM.LE.ZEROL) DENOM=ZEROL
   DETRAT=0.003+1.088/DENOM
   DETRAT=DETRAT*PK
6  RETURN
   END

C  SUBROUTINE ELEV(X,Y,TMAC)
C
C  SUBROUTINE LEV DETERMINES THE TERRAIN ELEVATION FOR A GIVEN
C  SET OF X, Y COORDINATES. THIS FUNCTION IS USED IN CONJUNCTION
C  WITH THE LOS SUBROUTINE IN COMPUTING LINE-OF-SIGHT BETWEEN
C  OBSERVER AND TARGET.
C
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ ECC(100),PXX(100),PY(100),PXY(100),BASE
COMMON /HILLS/ NHILLS
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(150),KTREP
COMMON /GRID/ LSTC(5,4),NC(5,4),LSTC(400),KCREP(150)
DATA GSIZE/1000./
C  FUNCTION TO COMPUTE TERRAIN ELEVATION FOR GIVEN X, Y COORDINATES.
ZMAX=BASE
IX=1+IFIX(X/GSIZE)
IY=1+IFIX(Y/GSIZE)
IF(NHL(IX,IY).EQ.0) GO TO 150
LS=LST(IX,IY)
LEND=LS+NHL(IX,IY)-1
DO 100 L=LS,LEND
  I=LISTH(L)
  QX=X-XC(I)
  QY=Y-YC(I)
  QXSQ=QX*QX
  QYSQ=QY*QY
  QXY=QX*QY
  FACTOR=PX(X(I)*QXSQ+PY(Y(I)*QYSQ+PXY(I)*QXY
  IF(FACTOR.LT.-3.) GO TO 100
  HT=PEAK(I)*EXP(FACTOR)
  IF(HT.LE.ZMAX) GO TO 100

```



```

ZMAX=HT
CONTINUE
100 TMAC=ZMAX
150 RETURN
END

C
SUBROUTINE STOCH(I,RANGE,A)
C
C
SUBROUTINE STOCH DETERMINES THE ATTRITION COEFFICIENTS WHEN
A USER HAS SELECTED A STOCHASTIC ATTRITION OPTION. THE CALCULATION
IS A FUNCTION OF THE ORIGINAL STOCHASTICALLY DETERMINED ATTRITION
COEFFICIENT AS WELL AS A FUNCTION OF RANGE.
C
COMMON /GRP6/ ALPHA(6)
COMMON /GRP3/ NBU,FL(6),FO(6),NOI(3),XIC(3,200),YIC(3,200),
1 IDIR(3,200),AVSP,ISPD
1 IUSTAT(6),I(6),LOST(6,6),VISFRA,VISFRB,SIZEZK,
1 SIZEZTW,NT(6),NF(6),SRF,DISMAX,
INLOSC(6,6),VISFR(6,6),RMINTK,RMXTK,RMINTW,RMXTW,OP,TOWER,TNKFR,
1 PTT(3,3),RF,POA(6,6),APOA(6,6),LOA(6,6),NA(6),OFL(6),POL(6)
1 IF(I.EQ.2) GO TO 5003
A=ALPHA(I)*((1.0-RANGE/RMXTW)**2)
GO TO 5004
5003 A=ALPHA(I)*((1.0-RANGE/RMXTK)**2)
5004 RETURN
END

C
SUBROUTINE ETK(I,RANGE,T)
C
C
SUBROUTINE ETK COMPUTES THE EXPECTED TIME FOR A GIVEN FIRER TO
KILL A GIVEN TARGET. THE CALCULATION IS A FUNCTION OF RANGE,
TIME OF FLIGHT FOR A ROUND AND HIT AND KILL PROBABILITIES FOR
THE FIRING WEAPON SYSTEM. IT IS A NUMBER THAT IS USED IN THE
COMPUTATION OF THE DETERMINISTIC ATTRITION COEFFICIENTS.
C
COMMON /GRP2/ TA(2),T1(2),TH(2),TM(2),TF1(2),TF2(2),TF3(2),
1 P(2,6),PHH(2,6),PHM(2,6),PKH(2,6),TF(2)
1 IF(I.EQ.2) GOTO 5
TF(I)=TF1(I)
GOTO 6
5 IF(RANGE.GT.1000.0) GOTO 7
TF(I)=TF1(I)-(TF1(I)*(1000.0-RANGE)/1000.0)
GOTO 6
7 IF(RANGE.GT.2000.0) GOTO 8
TF(I)=TF2(I)-((TF2(I)-TF1(I))*(2000.0-RANGE)/1000.0)
GOTO 6
8 TF(I)=TF3(I)-((TF3(I)-TF2(I))*(3000.0-RANGE)/1000.0)
6 J=(RANGE+250.0)/500.0

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GRA15300
 GRA15310
 GRA15320
 GRA15330
 GRA15340
 GRA15350
 GRA15360
 GRA15370
 GRA15380
 GRA15390
 GRA15400
 GRA15410
 GRA15420
 GRA15430
 GRA15440
 GRA15450
 GRA15460
 GRA15470
 GRA15480
 GRA15490
 GRA15500
 GRA15510
 GRA15520
 GRA15530
 GRA15540
 GRA15550
 GRA15560
 GRA15570
 GRA15580
 GRA15590
 GRA15600
 GRA15610
 GRA15620
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 GRA15640
 GRA15650
 GRA15660
 GRA15670
 GRA15680
 GRA15690
 GRA15700
 GRA15710
 GRA15720
 GRA15730
 GRA15740
 GRA15750
 GRA15760
 GRA15770

GRA15780
 GRA15790
 GRA15800
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 GRA15820
 GRA15830
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 GRA16010
 GRA16020
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 GRA16120
 GRA16130
 GRA16140
 GRA16150
 GRA16160
 GRA16170
 GRA16180
 GRA16190
 GRA16200
 GRA16210
 GRA16220
 GRA16230
 GRA16240
 GRA16250

```

IF(J.GT.6) J=6
T=TA(I)+TI(I)-TH(I)+(TH(I)+IF(I))/PKH(I,J))+((TM(I)+TF(I))/
IPHM(I,J))*((1.0-PHH(I,J))/PKH(I,J)+PHH(I,J)-P(I,J))
RETURN
END
C
SUBROUTINE SORT(I,M)
C
C SUBROUTINE SORT IS USED TO SORT TARGETS IN ASCENDING RANGE
C ORDER. THIS IS USED TO DETERMINE THE PRIORITY OF A TARGET
C FOR FIRE ALLOCATION.
C
COMMON /GRP5/ LOT(6,6),ROT(6,6)
DO 19 J=1,M
IF(ROT(I,M).GE.ROT(I,J)) GOTO 19
21 R=ROT(I,J)
NN=LOT(I,J)
RCT(I,J)=ROT(I,M)
LOT(I,J)=LOT(I,M)
RCT(I,M)=R
LOT(I,M)=NN
19 CONTINUE
RETURN
END
C
SUBROUTINE KOVER(ZO,IMACT,SIZET,ZI,S,HTS,ZS,VISFRT)
C
C SUBROUTINE KOVER DETERMINES WHAT PORTION OF A PARTICULAR TARGET
C IS COVERED BY THE TERRAIN BETWEEN THE TARGET AND OBSERVER.
C THIS NUMBER IS USED IN THE DETECTION AND ATTRITION COMPUTATION.
C
IF(S.EQ.0.) GO TO 2000
IF(HTS.GE.ZS) GO TO 2050
HEXT=ZO+(HTS-ZO)/S
EVI1ST=AMAX1(HEXT,IMACT)
IF(EVI1ST.GE.ZI) GO TO 2050
IF(EVI1ST.LE.ZI-SIZET) RETURN
VIS=(ZI-EVI1ST)/SIZET
IF(VIS.LT.VISFRT) VISFRT=VIS
RETURN
2000 IF(HTS.LT.ZO) RETURN
2050 VISFRT=0.0
RETURN
END
C
SUBROUTINE LOS(XA,YA,TMACA,TMICA,SIZEA,XB,YB,TMACB,TMICB,SIZEB,
-LATOB,LBTOA,VISFRA,VISFRB)
C

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C SUBROUTINE LOS COMPUTES A PERCENT OF A TARGET VISIBLE TO A
C PARTICULAR OBSERVER, GIVEN THE COORDINATES OF BOTH.
C
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100),SPRD(100)
COMMON /HILLS/ ECC(100),PXX(100),PY(100),PXY(100),BASE
COMMON /HILLS/ NHILLS
COMMON /COVER/ CXC(150),CYC(150),CPEAK(150),CPXX(150),CPYY(150)
COMMON /COVER/ CPXY(150),NCVELS
COMMON /COUNTR/KH, KHW, KV, KN KGRS, KELL, KINT
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(150),KHREP(150),KTREP
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCREP(150)
COMMON /GRID/ LSTC(5,4),NC(5,4),LISTC(400),KCREP(150)
DIMENSION IGX(100),IGY(100),IEL(100),CS1(100),CS2(100)
DATA GSIZE/1000./
C SUBROUTINE TO COMPUTE FRACTION VISIBLE FOR OBSERVER TARGET PAIRS
VISFRA=1.
VISFRB=1.
XBA=XB-XA
YBA=YB-YA
IF((XBA.EQ.0.).AND.(YBA.EQ.0.)) RETURN
IF(SIZEA+TMICB.LE.0.) GO TO 510
IF(SIZEB+TMICB.LE.0.) GO TO 510
IF(TMICA.LT.0.) VISFRA=1.0+TMICA/SIZEA
IF(TMICB.LT.0.) VISFRB=1.0+TMICB/SIZEB
ZA=TMACA + TMICA + SIZEA
ZB=TMACB + TMICB + SIZEB
KTREP=KTREP+1
ZBA=ZB-ZA
XBASQ=XBA*XBA
YBASQ=YBA*YBA
XYBA=XBA*YBA
TWOXBA=2.*XBA
TWOYBA=2.*YBA
NGRSQ=0
IF(XBA) 110,95,100
95 XBA=0.1
100 ISGX=-1
XINC=GSIZE/XBA
GO TO 120
110 ISGX=1
XINC=-GSIZE/XBA
120 IF(YBA) 140,125,130
125 YBA=0.1
130 ISGY=-1
YINC=GSIZE/YBA
GO TO 150
140 ISGY=1
YINC=-GSIZE/YBA

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GRA16260
 GRA16270
 GRA16280
 GRA16290
 GRA16300
 GRA16310
 GRA16320
 GRA16330
 GRA16340
 GRA16350
 GRA16360
 GRA16370
 GRA16380
 GRA16390
 GRA16400
 GRA16410
 GRA16420
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 GRA17120
 GRA17130
 GRA17140
 GRA17150
 GRA17160
 GRA17170
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 GRA17190
 GRA17200
 GRA17210

```

150 IX=1+IFIX(XB/GSIZE)
    IY=1+IFIX(YB/GSIZE)
    XNEXT=GSIZE*(FLOAT(IX)+0.5*(ISGX-1.))
    YNEXT=GSIZE*(FLOAT(IY)+0.5*(ISGY-1.))
    XSTEP=(XB-XNEXT)/XBA
    YSTEP=(YB-YNEXT)/YBA
    NGRSQ=NGRSQ+1
    IGY(NGRSQ)=IX
    IF((XSTEP-GT.1.)-AND.(YSTEP-GT.1.)) GO TO 200
    IF(XSTEP-YSTEP) 170,180,190
    IX=IX+ISGX
    XSTEP=XSTEP+XINC
    GO TO 160
    IX=IX+ISGX
    XSTEP=XSTEP+XINC
    IY=IY+ISGY
    YSTEP=YSTEP+YINC
    GO TO 160
    KGRS=KGRS+NGRSQ
200 C GRID SQUARE LIST NOW COMPLETE IN IGY, IGY WITH NGRSQ ENTRIES
    C
    C NOW FIND WHICH COVER ELLIPSES TOUCH THE A TO B LINE.
    C CHECK ELEVATIONS AT S1 AND S2 FOR EACH SUCH ELLIPSE.
    NELS=0
    CHTMAX=0.
    IF(NCVELS.EQ.0) GOTO 270
    DO 260 K=1,NGRSQ
      IX=IGX(K)
      IY=IGY(K)
      N=NC(IX,IY)
      IF(N.EQ.0) GO TO 260
      LS=LSSTC(IX,IY)
      LEND=LS+N-1
      DO 250 L=LS,LEND
        KELL=KELL+1
        IC=LISTC(L)
        IF(KCREP(IC).EQ.KTREP)
          KCREP(IC)=KTREP
          RX=XA-CXC(IC)
          RY=YA-CYC(IC)
          PPXX=CPXX(IC)
          PPYY=CPYY(IC)
          PPXY=CPXY(IC)
          AA=PPXX*XBASQ+PPYY*YBASQ+PPXY*XYBA
          BB=PPXX*XTWOXBA*RX+PPYY*XTWOYBA*RY+PPXY*(RX*YBA+RY*XBA)
          CC=PPXX*RX*RX+PPYY*RY*RY+PPXY*RX*RY-1.0
          ARG=BB*BB-4.0*AA*CC
  
```


GRA17220
GRA17230
GRA17240
GRA17250
GRA17260
GRA17270
GRA17280
GRA17290
GRA17300
GRA17310
GRA17320
GRA17330
GRA17340
GRA17350
GRA17360
GRA17370
GRA17380
GRA17390
GRA17400
GRA17410
GRA17420
GRA17430
GRA17440
GRA17450
GRA17460
GRA17470
GRA17480
GRA17490
GRA17500
GRA17510
GRA17520
GRA17530
GRA17540
GRA17550
GRA17560
GRA17570
GRA17580
GRA17590
GRA17600
GRA17610
GRA17620
GRA17630
GRA17640
GRA17650
GRA17660
GRA17670
GRA17680
GRA17690

```

IF(ARG.LE.0.) GO TO 250
SQ=SQRT(ARG)
S1=-(BB+SQ)/(2.0*AA)
S2=(SQ-BB)/(2.0*AA)
IF(S1.GE.1.) GO TO 250
IF(S2.LE.0.) GO TO 250
IF(S1.LE.0.) GO TO 510
IF(S2.GE.1.) GO TO 510
CHECK LOS AT S1 AND S2
C NOW
KINT=KINT+1
CPK=CPEAK(IC)
XS=XAS+S2*XBA
YS=YAS+S2*YBA
CALL ELEV(XS,YS,HTS)
HTS=HTS+CPK
ZS=ZAS+S2*ZBA
IF(LATOB.EQ.0) GO TO 210
CALL KOVER(ZA,TMACB,SIZEB,ZB,S2,HTS,ZS,VISFRB)
IF(VISFRB.LE.0.) GO TO 510
IF(LBTQA.EQ.0) GO TO 220
S=1.-S2
CALL KOVER(ZB,TMACA,SIZEA,ZA,S,HTS,ZS,VISFRA)
IF(VISFRA.LE.0.) GO TO 510
XS=XAS+S1*XBA
YS=YAS+S1*YBA
CALL ELEV(XS,YS,HTS)
HTS=HTS+CPK
ZS=ZAS+S1*ZBA
IF(LATOB.EQ.0) GO TO 230
CALL KOVER(ZA,TMACB,SIZEB,ZB,S1,HTS,ZS,VISFRB)
IF(VISFRB.LE.0.) GO TO 510
IF(LBTQA.EQ.0) GO TO 240
S=1.0-S1
CALL KOVER(ZB,TMACA,SIZEA,ZA,S,HTS,ZS,VISFRA)
IF(VISFRA.LE.0.) GO TO 510
NELS=NELS+1
IEL(NELS)=IC
CS1(NELS)=S1
CS2(NELS)=S2
IF(CPK.GT.CHTMAX) CHTMAX=CPK
250 CONTINUE
260 CONTINUE
C ALL ELLIPSES CHECKED
C
C NOW START ON THE HILLS
270 DO 600 K=1,NGRSQ
IX=IGX(K)
IY=IGY(K)

```


GRA17700
GRA17710
GRA17720
GRA17730
GRA17740
GRA17750
GRA17760
GRA17770
GRA17780
GRA17790
GRA17800
GRA17810
GRA17820
GRA17830
GRA17840
GRA17850
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GRA17870
GRA17880
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GRA17900
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GRA17980
GRA17990
GRA18000
GRA18010
GRA18020
GRA18030
GRA18040
GRA18050
GRA18060
GRA18070
GRA18080
GRA18090
GRA18100
GRA18110
GRA18120
GRA18130
GRA18140
GRA18150
GRA18160
GRA18170

```

IF(NHL(IX,IY).EQ.0) GO TO 600
LS=LST(IX,IY)
LEND=LS+NHL(IX,IY) -1
DO 500 L=LS,LEND
I=LSTH(L)
IF(KHREP(I).EQ.KTREP) GO TO 500
KHREP(I)=KTREP
C PROCESSING FOR HILL I STARTS HERE
KH=KH+1
C COMPUTE W = TOP OF THIS HILL ALONG O-T LINE
C
TRX=XA-XC(I)
TRY=YA-YC(I)
TPXX=PX(X(I))
TPYY=PY(Y(I))
TPXY=PX(Y(I))
FQ=TWOXBA*TPXX*TRX+TWOYBA*TPYY*TRY+TPXY*(TRX*YBA+TRY*XBA)
GQ=TPXX*XBASQ+TPYY*YBASQ+TPXY*XYBA
IF(GQ.EQ.0.) GO TO 500
W=-FQ/(2.*GQ)
IF(ABS(W).GT.5.) GO TO 500
FSQ=FQ*FQ
EQ=TPXX*TRX+TPYY*TRY+TPXY*TRX*TRY
C
POWER=EQ-FSQ/(4.*GQ)
IF(POWER.LT.-3.) GO TO 500
HHW=PEAK(I)*EXP(POWER)
KHW=KHW+1
IF(HHW.LE.BASE) GO TO 500
ZW=ZA+W*ZBA
IF((W.LT.0.) OR.(W.GT.1.)) GO TO 300
IF(HHW.GE.ZW) GO TO 510
CVHTW=0.
IF(NELS.EQ.0) GO TO 300
DO 280 M=1,NELS
IF((CS1(M).GE.W).OR.(CS2(M).LE.W)) GO TO 280
IC=IEL(M)
IF(CVHTW.LT.CPEAK(IC)) CVHTW=CPEAK(IC)
280 CONTINUE
IF((HHW+CVHTW).GE.ZW) GO TO 510
300 IF(HHW+CHTMAX.LT.AMIN1(ZA-SIZEA,ZB-SIZEB)) GO TO 500
C IF WE GET TO HERE THEN NEED TO FIND LOWEST SIGHT LINE OVER HILL
C NEWTON ITERATION A TO B GIVING VISFRB
IF(LATOB.EQ.0) GO TO 400
KV=KV+1
V=W
HHV=HHW
NCT=0

```



```

330 FV=FQ*V
      TWOGV=2.*GQ*V
      FCNV=Z A+HHV*(TWOGV*V+V-1.)
      KN=KN+1
      FACTOR=(TWOGV*TWOGV+2.*(GQ+TWOGV*FQ)+FSQ)
      DFCNV=HHV*V*FACTOR
      IF (ABS(DFCNV) .LT. 1.E-10) GO TO 350
      V=V-FCNV/DFCNV
      FV=FQ*V
      TWOGV=2.*GQ*V
      POWER = EQ+V+GQ*V*V
      IF (POWER .LT. -3.) GO TO 400
      HHV=PEAK(I)*EXP(POWER)
      DHHV=HHV*(FQ+TWOGV)
      ELV=Z A+DHHV*V
      IF (ABS(HHV-ELV) .LT. 1.) GO TO 350
      NCT=NCT+1
      IF (NCT .LT. 10) GO TO 330
      IF ((V .LT. 0.) .OR. (V .GT. 1.)) GO TO 400
      CVHTV=0.
      IF (NELS .EQ. 0) GO TO 390
      DO 380 M=1, NEL
      IF ((CS1(M).GE.V) .OR. (CS2(M).LE.V)) GO TO 380
      IC=IEL(M)
      IF (CVHTV .LT. CPEAK(IC)) CVHTV=CPEAK(IC)
      CONTINUE
      HTV=HHV+CVHTV
      ZV=Z A+V*ZBA
      CALL KOVER(ZA, TMACB, SIZEB, ZB, V, HTV, ZV, VISFRB)
      IF (VISFRB .LE. 0.) GO TO 510
      C NEWTON ITERATION B TO A GIVING VISFRA
      400 IF (ABS(V) .GT. 5.) GO TO 400
      IF (LBTOA .EQ. 0) GO TO 500
      KV=KV+1
      V=W
      VM1=V-1.
      HHV=HHW
      NCT=0
      FV=FQ*V
      TWOGV=2.*GQ*V
      FCNV=ZB+HHV*((FQ+TWOGV)*VM1-1.)
      KN=KN+1
      FACTOR=(TWOGV*TWOGV+2.*(GQ+TWOGV*FQ)+FSQ)
      DFCNV=HHV*VM1*FACTOR
      IF (ABS(DFCNV) .LT. 1.E-10) GO TO 450
      V=V-FCNV/DFCNV
      IF (ABS(V) .GT. 5.) GO TO 500
      VM1=V-1.

```

GRA18180
 GRA18190
 GRA18200
 GRA18210
 GRA18220
 GRA18230
 GRA18240
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 GRA18290
 GRA18300
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GRA18900
GRA18910
GRA18920
GRA18930
GRA18940
GRA18950

```

FV=FQ*V
TWOGV=2.*GQ*V
POWER = EQ+FV+GQ*V*V
IF (POWER .LT. -3.) GO TO 500
HHV=PEAK(I)*EXP(POWER)
DHHV=HHV*(FQ+TWOGV)
ELV=ZB+DHHV*VM1
IF (ABS(HHV-ELV) .LT. 1.) GO TO 450
NCT=NCT+1
IF (NCT.LT.10) GO TO 430
IF ((V.LT.0.).OR.(V.GT.1.)) GO TO 500
CVHTV=0.
IF (NELS.EQ.0) GO TO 490
DO 480 M=1,NELS
IF ((CS1(M).GE.V).OR.(CS2(M).LE.V))GO TO 480
IC=IEL(M)
IF (CVHTV.LT.CPEAK(IC)) CVHTV=CPEAK(IC)
CONTINUE
HTV=HHV+CVHTV
ZV=ZA+V*ZBA
S=-VM1
CALL KOVER(ZB,TMACA,SIZEA,ZA,S,HTV,ZV,VISFRA)
IF (VISFRA.LE.0.) GO TO 510
CONTINUE
CONTINUE
RETURN
VISFRA=0.
VISFRB=0.
RETURN
END

```

450

480

490

500

600

510

PLOTTING PROGRAM FOR TERRAIN CONTOUR LINE

96

XXH(4)=5000.
YYH(4)=1000.

CC C USING THE BISECTION SEARCH METHOD, FIND THE LOCATION
C WHICH HAS A ELEVATION, I, E. 20, 40, ... ETC.

ME=5
YELTA=20.
XELTA=5.
XEL=1000.
YEL=1000.
YCON=1000
XEND=5000
YEND=4000.
991 CALL ELEV(XEL,YEL,ZNEW)
TELTA=YELTA
NVAL1=IFIX(ZNEW/20.)
717 ZOLD=ZNEW
727 YEL=YEL+YELTA
IF(YEL.LT.YEND) GO TO 777
XEL=XEL+5.
IF(XEL.EQ.XEND) GO TO 333
YEL=YCON
GO TO 991
777 CALL ELEV(XEL,YEL,ZNEW)
NVAL2=IFIX(ZNEW/20.)
IZZ=IABS(NVAL2-NVAL1)
IF(IZZ.GE.1) GO TO 788
NVAL1=NVAL2
GO TO 717
788 KVAL=NVAL2
YRES=YEL
IF(NVAL2.GT.NVAL1) GO TO 630
ZVAL=NVAL1*20.
NK=1
TELTA=YELTA
631 YEL=YEL-TELTA/2.
632 CALL ELEV(XEL,YEL,ZNEW)
IF(ZNEW.LT.ZVAL+0.1.AND.ZNEW.GT.ZVAL-0.1) GO TO 800
IF(NK.GT.4) GO TO 800
ZOLD=ZNEW
TELTA=TELTA/2.
NK=NK+1
IF(ZNEW.LT.ZVAL) GO TO 631
YEL=YEL+TELTA/2.0
GO TO 632

CC C CALCULATE INCREASING ELEVATION

630 ZVAL=NVAL2*20.
NK=1
TELTA=YELTA
642 YEL=YEL-TELTA/2.0
643 CALL ELEV(XEL,YEL,ZNEW)
IF(ZNEW.LT.ZVAL+0.1.AND.ZNEW.GT.ZVAL-0.1) GO TO 800
IF(NK.GT.4) GO TO 800
ZOLD=ZNEW
TELTA=TELTA/2.0
NK=NK+1
IF(ZNEW.GT.ZVAL) GO TO 642
YEL=YEL+TELTA/2.0
GO TO 643

CC C COLLECT ELEVATION COORINATE DATA WHICH IS WANTED TO BE
C PLOTTED.

800 IF(ZVAL.LT.20.) GO TO 189


```

IF(ZVAL.GT.140.) GO TO 189
IF(ZVAL.NE.20.AND.ZVAL.LT.100.) GO TO 189
XXH(ME)=XEL
YYH(ME)=YEL
ME=ME+1
189 NVAL1=KVAL
YEL=YRES
GO TO 727
333 NP=ME-1
CALL PLOTG(XXH,YYH,NP,1,0,75,'X-AXIS LABEL',12,
1 'Y-AXIS LABEL',12,XMIN,XMAX,YMIN,YMAX,8.,6.)
CALL PLOT(0.,0.,999)
STOP
END
SUBROUTINE ELEV(X,Y,TMAC)

```

C
C
C

COMPUTE THE ELEVATION FOR A GIVEN X,Y COORDINATE

```

IMPLICIT REAL*4(A-H,O-Z)
COMMON /HILLS/ XC(100),YC(100),PEAK(100),ANGH(100)
COMMON /HILLS/ SPRD(100),ECC(100),PXX(100),PYY(100)
COMMON /HILLS/ PXY(100),BASE,NHILLS
COMMON /GRID/ LST(5,4),NHL(5,4),LISTH(100),KHREP(100)
COMMON /GRID/ KTREP
DATA GSIZE/1000./
ZMAX=BASE
IX=1+IFIX(X/GSIZE)
IY=1+IFIX(Y/GSIZE)
IF(NHL(IX,IY).EQ.0) GO TO 150
LS=LST(IX,IY)
LEND=LS+NHL(IX,IY)-1
DO 100 L=LS,LEND
I=LISTH(L)
QX=X-XC(I)
QY=Y-YC(I)
QXSQ=QX*QX
QYSQ=QY*QY
QXY=QX*QY
FACTOR=PXX(I)*QXSQ+PYY(I)*QYSQ+PXY(I)*QXY
IF(FACTOR.LT.-3.) GO TO 100
HT=PEAK(I)*EXP(FACTOR)
IF(HT.LE.ZMAX) GO TO 100
ZMAX=HT
100 CONTINUE
150 TMAC=ZMAX
RETURN
END

```


LIST OF REFERENCES

1. Bonder, S., "The Lanchester Attrition-Rate Coefficient," Operations Research, v. 15, p. 221-232, May 1967.
2. Bonder, S., "An Overview of Land Battle Modeling in the U.S." In: Proceedings 13th U.S. Army Operations Research Symposium, pp. 73-77, 1974.
3. Chardwick, D.L., The Evaluation of Design and Employment Alternative for the LVA: A Modelling Strategy, M.S. Thesis, Naval Postgraduate School, Monterey, California, September 1978.
4. Farmer, W.T., A Survey of Approaches to the Modeling of Land Combat, M.S. Thesis, Naval Postgraduate School, Monterey, California, June 1980.
5. Hartman, J.K., Parametric Terrain and Line-of-Sight Modeling in the STAR Combat Model, Naval Postgraduate School, Monterey, California, 1979.
6. Mills, G.M., The Enrichment of Smoller's Model of Land Combat, M.S. Thesis, Naval Postgraduate School, Monterey, California, September 1980.
7. Morris, W.T., "On the Art of Modeling," Management Science 13, B707-B717, August 1967.
8. Needels, C.G., Parameterization of Terrain in Army Combat Models, M.S. Thesis, Naval Postgraduate School, Monterey, California, March 1976.
9. Smoller, J., Operational Lanchester-type Model of Small Unit Land Combat, M.S. Thesis, Naval Postgraduate School, Monterey, California, September 1979.
10. Taylor, J.G., Force-on-Force Attrition Modeling, Military Application Section of Operations Research of America, January 1980.
11. Wallace, W.S., and Hagewood, E.G., Simulation of Tactical Alternative Responses (STAR), M.S. Thesis, Naval Postgraduate School, Monterey, California, December 1978.

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